

MOVPE growth and characterization of *a*-plane AlGaIn over the entire composition range

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We report the metal organic vapor phase epitaxy (MOVPE) growth and characterization of non-polar (11 $\bar{2}$ 0) *a*-plane Al_{1-x}Ga_xIn on (1102) *r*-plane sapphire substrates over the entire composition range. Al_{1-x}Ga_xIn samples with $x = 0, 0.18, 0.38, 0.46, 0.66,$ and 1.0 thick layers and with $x = 0, 0.18, 0.38, 0.46, 0.66,$ and 1.0 have been grown on *r*-plane sapphire substrates. The layer quality can be improved by using a 3-stage AlN nucleation layer and appropriate V/III ratio switching following nuclea-

1 Introduction AlGaIn, a wide bandgap semiconductor material, is very promising for UV-optoelectronics and high frequency devices. Nitride epilayers grown along the (0001) *c*-axis of the wurtzite crystal structure, suffer from undesirable spontaneous and piezoelectric polarization fields which impair device performance [1]. Thus, growth along “non polar” (11 $\bar{2}$ 0) *a*-plane and (1100) *m*-plane ($\perp c$ -axis) is being extensively pursued. Non-polar *a*-plane GaIn layers have been grown on *r*-plane sapphire using different techniques [2–4], and there are a few reports of MOVPE grown *a*-plane AlGaIn [5, 6]. From studies on *c*-plane AlGaIn, it is known [7] that high quality epilayers are easier to grow on thick GaN buffers. However, deep UV LEDs ($\lambda \leq 365$ nm), require AlGaIn to be grown on transparent AlN buffer layers. Gas-phase reactions among precursors, low surface mobility of Al adatoms, and high sensitivity to V/III ratio and temperature make high quality AlGaIn growth a challenge. In this Letter we present, to the best of our knowledge, the first synthesis of crack-free, *a*-plane AlGaIn epilayers over the entire alloy composition via MOVPE.

2 Experiment AlGaIn epilayers were grown via MOVPE in a 3 × 2” closed-coupled showerhead reactor using trimethylgallium (TMGa), trimethylaluminum (TMAI) and ammonia (NH₃) precursors. For comparison between *a*-plane and *c*-plane AlGaIn, both *r*-plane and *c*-plane sapphire were loaded in the same run. Improved layer quality was obtained using a 3-stage AlN nucleation layer – sequential deposition of 10 nm at 700 °C, 35 nm at 900 °C, and 35 nm at 1040 °C, at a V/III ratio of 1600. A set of 0.8 μm thick Al_{1-x}Ga_xIn samples with $x_{\text{gas}} = 0, 0.2, 0.4, 0.5, 0.7, 1.0$ was grown at 1040 °C, V/III = 3000 and pressure 50 Torr. To change the alloy composition we varied the TMGa flow from 0 to 150 μmol/min at a fixed TMAI flow (28.5 μmol/min). Structural characterization of the epilayers was performed using a Philips X’PERT™ high resolution X-ray diffractometer with an asymmetric triple-axis analyzer and symmetric Ge(220) hybrid monochromator. Absorption measurements on backside polished samples were used to estimate the bandgap. The surface morphology was studied by optical interference contrast and atomic force microscopy.

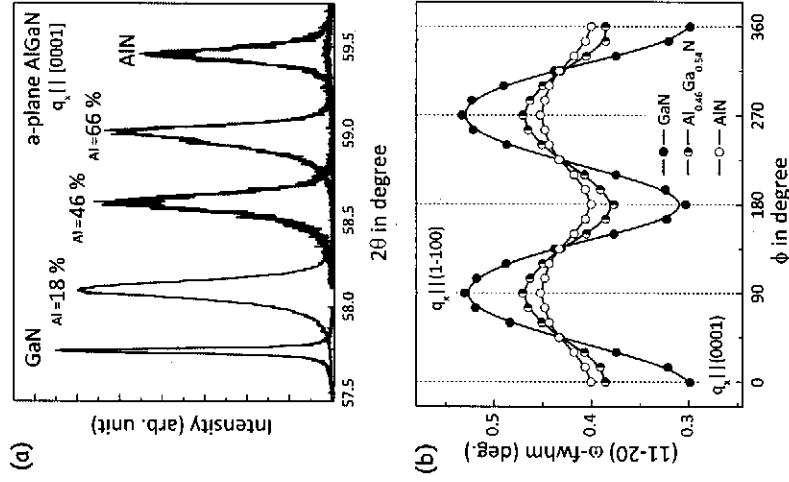


Figure 1 (online colour at: www.pss-rapid.com) (a) $\omega/2\theta$ X-ray scan of a series of *a*-plane AlGaIn samples with $x_{\text{solid}} = 0, 0.18, 0.46, 0.66, 1.0$ at $q_x \parallel [0001]$. (b) (1120) ω -fwhm as a function of in-plane rotation (ϕ) for three selected AlGaIn samples showing the in-plane anisotropic mosaicity, which decreases with increasing Al content.

3 Results Figure 1(a) shows $\omega/2\theta$ X-ray scans of the *a*-plane AlGaIn samples over the entire composition range. The GaN profile is very sharp, with peak widths of AlGaIn layers being relatively broad in comparison. Also the (1120) ω -fwhm (along *c*-axis) increases with the increase in Al content. In case of AlGaIn growth, Al adatoms have lesser surface mobility and larger sticking coefficient compared to the Ga atoms and are less likely to migrate to step edges and form smooth layers in a 2D growth mode [8]. The crystalline quality of the epilayers hence degrades on the addition of Al. The tendency towards island growth resulting in rougher layers is known from studies on *c*-plane AlGaIn, the inherent anisotropy of the *a*-plane surface makes the situation more complex.

All the AlGaIn epilayers show an in-plane anisotropy in the crystalline mosaicity, i.e., the (1120) ω -fwhm varies periodically as a function of in-plane rotation (ϕ) as shown in Fig. 1(b). The (1120) ω -fwhm value is maximum when the scattering plane is along the *m*-direction ($q_x \parallel [1100]$) and is minimum when the scattering plane lies along the *c*-direction ($q_x \parallel [0001]$). The (1120) $\omega/2\theta$ -fwhm and the (2θ) peak positions themselves do not change with the rotation ϕ . Figure 1(b) plots the (1120) ω -fwhm for GaIn, Al_{0.46}Ga_{0.54}N and AlN. This anisotropy strongly depends on

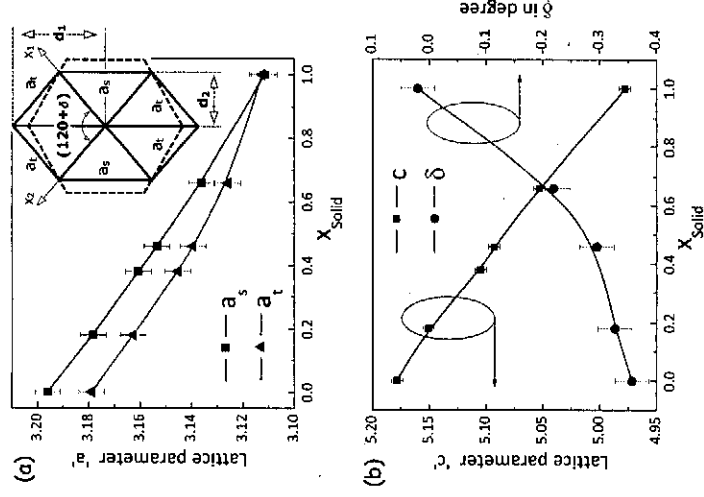


Figure 2 (online colour at: www.pss-rapid.com) (a) Variation in the sidewall (a_s) and top (a_t) lattice parameters as a function of Al incorporation x_{solid} . Inset: schematic diagram of the distorted hexagonal unit cell basal-plane. (b) Variation of *c*-axis lattice parameter and δ , the deviation from the 120° angle between the basal plane unit vectors as a function of x_{solid} . (Negative values of δ indicate angles $< 120^\circ$.)

the Al content. GaIn layers show the maximum anisotropy, which decreases on increasing Al incorporation. On *a*-plane oriented surfaces, the adatoms have larger incorporation probability and diffusion length along the [0001] direction [4]. This allows them a greater chance to find energetically favored positions and leads to a slightly faster growth rate and smaller ω -fwhm along the [0001] *c*-direction compared to [1100] *m*-direction. It also results in a striated surface morphology as seen in optical interference contrast microscopy. The anisotropy reduces with the Al incorporation because of the smaller diffusion length of Al adatoms compared to Ga. The smaller diffusion length of Al also explains the increased roughness of AlGaIn layers compared to GaIn: the RMS roughness values for GaIn and AlN measured from $2 \times 2 \mu\text{m}^2$ AFM scans are 4 nm and 18 nm, respectively. The microstructure and the anisotropy may also be influenced by the basal plane stacking fault density, the (1120) reflection is however not sensitive to such defects [9].

For *c*-plane oriented films, an AlGaIn epilayer on AlN is under uniform biaxial strain making the determination of lattice parameter and estimation of solid-phase Al incorporation (x_{solid}) relatively straightforward [10, 11]. However, for *a*-plane oriented films, the AlGaIn epilayer on AlN buffer is under *anisotropic* biaxial strain as the lattice

mismatch and thermal expansion coefficients along the [0001] *c*-direction and [100] *m*-direction are different. That results in an orthorhombic distortion of the hexagonal unit cell, making lattice parameter measurements and Al composition determination nontrivial [12, 13]. We have developed a detailed procedure for estimating the lattice parameters of orthorhombic distorted structures and an expression for estimating x_{solid} for such ternary alloys [14]. A schematic diagram of the distorted hexagonal unit cell is shown in the inset of Fig. 2(a). In this case the inter-planer distances can be described by $1/d_{hkl}^2 = (h^2 + k^2 - 2hk \cos \gamma)/(a \sin \gamma)^2 + l^2/c^2$, where $\gamma = 120^\circ + \delta$ is the angle between the x_1 and x_2 axes, $\alpha = \beta = 90^\circ$ [15]. Unlike a regular hexagon, we need two different lattice parameters a_s (sidewall) and a_t (top) for a complete description of the distorted basal plane. Figure 2 shows that the lattice parameters a_s , a_t , and c decrease whereas δ increases as a function of x_{solid} . As x_{solid} increases, the anisotropic biaxial strain between AlGaIn layer and AlN buffer decreases, hence the value of $|a_s - a_t|$ and δ decrease monotonically. Using the lattice parameters, and incorporating the effects of strain, for small distortions ($\delta < 1^\circ$), x_{solid} can be expressed as

$$x_{\text{solid}} \approx \frac{(c_G - c) d_1 d_2 + \gamma_1 (d_{1G} - d_1) c d_2 + \gamma_2 (d_{2G} - d_2) c d_1}{(c_G - c_A) d_1 d_2 + \gamma_1 (d_{1G} - d_{1A}) c d_2 + \gamma_2 (d_{2G} - d_{2A}) c d_1},$$

where $d_1 = 2d_{120} = (2a \sin \gamma) / \sqrt{2(1 - \cos \gamma)}$ and $d_2 = d_{100} = (a \sin \gamma) / \sqrt{2(1 + \cos \gamma)}$; a , c and γ are the lattice parameters of the distorted AlGaIn epilayer; subscripts *G* and *A* denote GaN and AlN, respectively (i.e., c_G is the *c*-lattice parameter of GaN); $\gamma_1 = C_{11}/C_{13}$ and $\gamma_2 = C_{12}/C_{13}$, where C_{11} , C_{12} , C_{13} are the elastic stiffness constants.

To verify the accuracy in x_{solid} estimated from the lattice parameters, we have also used optical transmission data to estimate x_{solid} . Figure 3 (inset) shows the transmission cut-off of *a*-plane AlGaIn epilayers of different compositions. The bandgap of AlGaIn can be expressed as $[10] E_g^{\text{AlGaIn}} = x E_g^{\text{AlN}} + (1-x) E_g^{\text{GaN}} + bx(1-x)$, where E_g^{GaN} , E_g^{AlN} , and E_g^{AlGaIn} are the bandgaps of GaN, AlN and AlGaIn, respectively. We use $b = 1 \pm 0.2$ eV, a value determined from our *c*-plane AlGaIn samples and similar to that reported in literature [16], to estimate x_{solid} for the *a*-plane AlGaIn. The effect of anisotropic biaxial strain on the bandgap is estimated from data available for *c*-plane GaN [17]; for the strains measured in our samples the change in bandgap is $E_g \approx 20$ meV, corresponding to a change in x_{solid} of about $\pm 1\%$. The values of x_{solid} estimated from the X-ray data via strain-tensor calculations and from optical transmission are within 2%, providing a reasonable error-bound on the Al content.

Figure 3 shows the variation of x_{solid} as a function of gas-phase Al concentration (x_{gas}). A near-linear behavior indicates minimal gas phase pre-reactions. For the same x_{gas} , the Al incorporation is slightly larger in *c*-plane films than in *a*-plane films. For mass transport limited growth, x_{solid} depends on the relative fluxes of Al and Ga atoms dif-

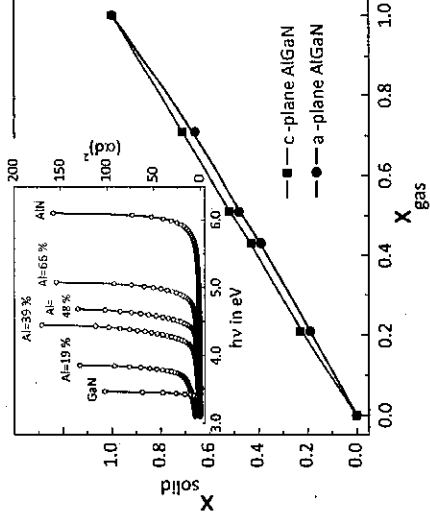


Figure 3 (online colour at: www.pss-rapid.com) Variation of Al incorporation in the epilayer, x_{solid} , as a function of $x_{\text{gas}} = \text{[TMAl]/[TMAl + TMGa]}$ ratio in the gas phase, for *c*- and *a*-plane samples. Inset: Square of the absorption coefficient-thickness product as a function of photon energy for the *a*-plane AlGaIn samples. The Al content determined from the absorption cut off values – $x_{\text{solid}} = 0, 0.19, 0.39, 0.48, 0.66, 1.0$ – is within 2% of that determined from analysis of lattice parameters.

fusing to the surface, which in the same growth run, are the same for the two surfaces. The lower solid phase Al incorporation for *a*-plane AlGaIn is probably due to differences in the relative sticking coefficients and incorporation probabilities for the two surfaces, further influenced by the *a*-plane surface anisotropy.

In conclusion we report the synthesis and characterization of *a*-plane AlGaIn epitaxial layers across the entire alloy composition range. The layers are mosaic and anisotropic due to an orthorhombic distortion in the hexagonal unit cell resulting from anisotropic biaxial strain. For such systems, we estimate solid phase Al incorporation using lattice parameters within reasonable accuracy. The demonstration of such AlGaIn layers would help to develop non-polar nitride based UV devices.

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