

Review

Sputtered transparent electrodes for optoelectronic devices: Induced damage and mitigation strategies

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SUMMARY

Transparent electrodes and metal contacts deposited by magnetron sputtering find applications in numerous state-of-the-art optoelectronic devices, such as solar cells and light-emitting diodes. However, the deposition of such thin films may damage underlying sensitive device layers due to plasma emission and particle impact. Inserting a buffer layer to shield against such damage is a common mitigation approach. We start this review by describing how sputtered transparent top electrodes have become archetypal for a broad range of optoelectronic devices and then discuss the possible detrimental consequences of sputter damage on device performance. Next, we review common buffer-layer materials in view of their processing-property-performance relationship. Finally, we discuss strategies to eliminate the buffer-layer requirement by implementing alternative, soft-landing deposition techniques for top electrodes. Our review highlights the critical issue of sputter damage for optoelectronic devices, formulates mitigation strategies, and provides cross-field learnings that can lead to more efficient and reliable optoelectronic devices aimed for commercialization.

INTRODUCTION

Optoelectronic devices, such as solar cells and light-emitting diodes (LEDs), are ubiquitous in modern society.¹ Such devices typically consist of a photoactive material, sandwiched between an electron transport layer (ETL) and hole transport layer (HTL), as well as two outer electrodes, of which at least the front electrode is usually highly transparent.² Examples of devices with such an architecture are silicon heterojunction (SHJ) solar cells,³ thin-film silicon solar cells,⁴ perovskite solar cells (PSCs),⁵ organic solar cells (OSCs),⁶ chalcogenide solar cells, colloidal quantum dots solar cells (QDSCs),⁷ organic LEDs (OLEDs),⁸ and quantum-dot LEDs (QLEDs).⁹ Transparent conductive oxides (TCOs) are the most established choice as transparent electrodes, as they can simultaneously feature high optical transparency and electrical conductivity, are usually robust, and are deposited using well-established deposition techniques.¹⁰

For the fabrication of TCOs, magnetron sputtering is the most widespread technique both for lab-scale and commercial devices.^{11–14} This vacuum-based deposition technique relies on the plasma excitation of a gas (usually Ar) that is ignited either via a direct current (DC) or radio frequency (RF) power source. The resulting

Progress and potential

Optoelectronic devices, such as solar cells and light-emitting diodes, as well as transparent electronic devices, rely on efficient light-matter interactions and usually require transparent top electrodes that are deposited onto a device layer stack. Magnetron sputtering, well established in the coating industry, is the most common technique to deposit such materials. Nevertheless, this process may result in irreversible damage to underlying sensitive layers because the deposition process involves high-energy particles and plasma emission. Several strategies are available to prevent such damage; some of these methods are common for various optoelectronic devices, while others have yet to be considered for specific applications. Taking inspiration across different research fields, we discuss how to choose adequate buffer layers for various optoelectronic devices as well as possible paths to eliminate their need via soft-landing methods for transparent electrodes.



plasma-related species bombard a target material, resulting in a transfer of particles from the target to the substrate. Sputtered TCOs offer excellent optoelectronic performance, high reproducibility, and additional functionalities (e.g., barrier properties against metal diffusion or humidity) due to the dense nature of most sputtered TCOs. However, the kinetic energy of the plasma particles, plasma emission, and processing-induced heat may harm underlying sensitive layers of the devices during the deposition.¹⁵ Layers susceptible to sputter damage can be either the underlying charge transport layers or the active materials, where structural changes, such as the breaking of chemical bonds, may deteriorate material properties, thereby compromising device performance and stability.^{16,17} Therefore, successful implementation of TCOs as top electrodes requires the minimization of sputter damage without jeopardizing film quality or throughput. As is addressed in this review, this may be accomplished either by utilizing additional thin-film layers that are resilient against sputter damage and do not incur device performance losses (here labeled as buffer layers, but also known as protective layers, interfacial layers, or blocking layers) or by finding alternative damage-free deposition techniques for TCOs.

Specifically, following a brief [introduction](#) about transparent electrodes as commonly used in optoelectronic devices, we discuss possible causes of device damage during sputter deposition of these transparent electrodes, followed by a review of materials and methods to fabricate protective buffer layers, focusing on their processing-property-performance relation and appropriateness for a given device technology. Moreover, from a performance and cost perspective, buffer-layer elimination may be desirable (as their deposition adds an additional processing step; their presence can also impose a carrier-transport barrier in contact stacks). This, however, requires process sophistication or even the replacement of magnetron sputtering by alternative soft-landing deposition techniques to fabricate these transparent electrodes. We discuss available alternative deposition methods and provide an outlook for further developing damage-free deposition of TCOs on optoelectronic devices that feature process-sensitive layers.

TRANSPARENT TOP ELECTRODE REQUIREMENTS FOR OPTOELECTRONIC DEVICES

In archetypal solar cells and top-emitting (or upwards-emitting) LEDs, an ideal transparent top electrode must effectively extract or inject charges while exhibiting minimal optical and electrical losses. Independent from the application, all transparent electrode materials should combine (1) transparency in the spectral range of absorption or emission of the device, (2) high lateral conductivity, (3) low-resistance Ohmic contact with adjacent layers, (4) chemical stability, and (5) low processing impact to the underlying layers. Specifically, TCO films capping the device layer stack as transparent electrodes may also improve protection against moisture ingress.¹⁸ To better understand the necessity of an additional buffer layer to accomplish these criteria, this section first discusses the formation of transparent electrodes and their impact at the device level. Here, we give a nonexhaustive description of commonly used transparent electrodes with perspective of performance and robustness relation. For a detailed investigation of the optoelectronic properties of TEs, we encourage readers to check the review by Morales-Masis et al.¹⁰

Types of transparent electrodes

One simple approach to obtain a transparent electrode consists of thermally evaporating ultrathin (<10 nm) metallic films such as Ag, Au, or Al, which can provide a high lateral conductivity and are suitable for flexible devices;¹⁰ however, a low

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percolation threshold is desirable to ensure high transparency. The percolation threshold defines the minimum material coverage (continuous network of connections between particles or wires) required to provide adequate conductivity while offering sufficient optical transparency. This value is usually high for metal films, implying that dense (continuous) films are needed to ensure a high conductivity at the expense of reduced optical transparency. Presynthesized metal nanowires (NWs) can be deposited as an alternative to metal thin films, which offer a lower percolation threshold.¹⁹ However, metal NWs (e.g., synthesized from Ag, Cu, Au) usually exhibit poor adhesion as well as a high contact resistance with their adjacent materials and a poor chemical and environmental stability due to atmospheric corrosion driven by their large surface-to-volume ratio. A promising approach to overcome the mechanical stability issues of metal NWs is to embed them into a polymer matrix.²⁰ A similar approach is used for hybrid polymer/carbon-nanomaterials as transparent electrodes.²¹ In this sense, carbon-based materials, such as carbon nanotubes (CNTs) and graphene, have gained much interest as stand-alone transparent electrodes due to their excellent electrical properties, combined with high flexibility and chemical stability, as well the potential to deposit such layers using simple processing techniques (such as ink-jet printing). Nevertheless, even though some hybrid transparent electrodes based on Ag-NW/CNT have reached the requirements for the anodes of efficient OLED displays, the scaled processing of carbon-based transparent electrodes over large areas is yet to be demonstrated.^{10,22}

Sandwiching thin metal films (Ag, Au, Cu with ≤ 10 nm in thickness) into dielectric metal oxides (WO_x , V_2O_x , MoO_x) is another hybrid approach with attractive properties for certain applications; such dielectric/metal/dielectric (DMD) multilayer structures have yielded decent transparency ($\geq 70\%$) and conductivity characteristics close to conventional TCOs.^{23–27} DMD electrodes provide better elasticity than crystalline TCO electrodes (e.g., indium tin oxide [ITO]) due to the good flexibility of intermediate metal layers, making these electrodes advantageous to utilize in flexible optoelectronics. The requirement of delicate thickness control over the layers to achieve optimum transparency, as well as the stability issues of metal films (Cu, Ag) and their high cost (Au, Ag; need for multiple depositions) are concerns yet to be solved for DMD electrodes. To learn more about DMD electrodes, we also encourage readers to consult previously published reviews by Cao et al.,²⁸ and Kim and Lee.²³

As an alternative to these approaches, conductive polymers can be employed as low-cost and flexible transparent electrodes. However, to date, poly(3,4-ethylenedioxythiophene) (PEDOT) is the only state-of-the-art transparent conducting polymer with suitable conductivities to serve as an electrode.^{22,29} This conjugated polymer can be doped by partial oxidation of the thiophene in the liquid or vapor phase. The former is commonly done in the presence of poly(styrene sulfonate) (PSS), acting as the counter ion and stabilizer for the doped PEDOT. However, the hygroscopic and corrosive nature of PEDOT:PSS might cause device degradation under operation, hence a short life span.^{30,31} Nevertheless, utilizing oxidative chemical vapor deposition (oCVD) followed by acid treatment can give highly conductive (6259 S/cm) and air-stable PEDOT films.³²

Despite the development of these alternative approaches in the lab environment, most of the state-of-the-art solar cells and top-emitting organic/QD LEDs for commercial applications rely on the deposition of TCOs as transparent electrodes at the final stage of device processing. Critical advantages of TCOs are their well-established deposition methods with high throughput, high stability, and, critically, high electrical mobility

Table 1. Comparison of transparent electrodes for various optoelectronic devices

Materials	Device applications	Deposition methods	Benefits	Drawbacks
TCOs	silicon and thin-film solar cells, PSCs, OSCs, LEDs	sputtering, PLD ^a , CVD ^b , ALD ^c , solution processing	low resistivity and high transparency, well-established fabrication, excellent thermal and chemical stability	expensive, sputtered TCOs: damage to layers underneath, in-based TCOs: the scarcity of indium
carbon nanotubes	PSCs, OSCs	solution transfer, CVD	high conductivity and transparency, low cost	expensive, limited dispersibility, low conductivity, poor stability
graphene sheets	PSCs	CVD, thin film transfer techniques	high conductivity and transparency	low work function, poor doping stability, uniformity over large areas
thin metal films	LEDs, OSCs	evaporation, sputtering	simple process	trade-off between conductivity and transparency, poor stability, sputtered: damage to layers underneath
metal nanowires	PSCs, OSCs	solution processing	good conductivity	high roughness, poor adhesion, high contact resistance
dielectric/metal/dielectric multilayers	PSCs, OSCs, LEDs	Evaporation	good conductivity, transparency, and high mechanical flexibility	demanding precise thickness control of the multilayer stack, possible low stability due to metal interlayer films
conductive polymers	OSCs, LEDs	solution processing, CVD	low cost, flexible conductors	hygroscopic nature, poor stability

^aPulsed laser deposition.

^bChemical vapor deposition.

^cAtomic layer deposition.

coupled with high transparency. TCOs with especially high carrier mobilities include those based primarily on indium oxide, similar to the archetypical TCO ITO; emerging high carrier mobility TCOs in this category are hydrogen-doped indium oxide (IO:H), tungsten-doped indium oxide (IWO), and Zr-doped indium oxide (IZRO).^{11–14} Most of these TCOs are polycrystalline, even though certain variants such as indium zinc oxide (IZO) are amorphous, with excellent optoelectronic properties and outstanding temperature resilience.³³ For all listed TCOs, the most common deposition technique is sputtering. However, sputtering TCOs on top of the photoactive and other functional layers may set physical and chemical limitations, as discussed in the following section. Due to the widespread use of sputtered TCOs and metal oxides and the known challenges regarding sputtering damage, we focus the rest of the section on sputter deposition of TCOs. The comparison between the discussed alternative transparent electrodes is summarized in [Table 1](#).

Origins of damage during magnetron sputtering of TCOs

To identify the root causes of damage incurred by TCO sputtering onto sensitive layers, the working mechanism of the sputtering process should be understood. Elaborate descriptions of sputtering processes can be found in dedicated literature;^{34–37} here we briefly summarize the main principles of the deposition method with relevance to damage during sputtering. Sputtering is a nonthermal, plasma-assisted physical vapor deposition (PVD) method that involves ejecting atoms or molecules from a bulk target material (cathode) onto a substrate (anode) by momentum transfer, caused by the bombardment of plasma-excited high-energy particles (usually Ar ions). This process is typically performed in a low-pressure (<5 mammalian target of rapamycin) environment, where the sputtered particles suffer negligible gas-phase collisions. The ejected material is then directed onto a substrate to form a thin film, as sketched in [Figure 1](#). In magnetron sputtering, the plasma discharge is sustained in close vicinity of the target by magnetic confinement of the electrons. In contrast to the electrons, the ejected ions and neutral particles are barely influenced by the magnetic field.¹⁹

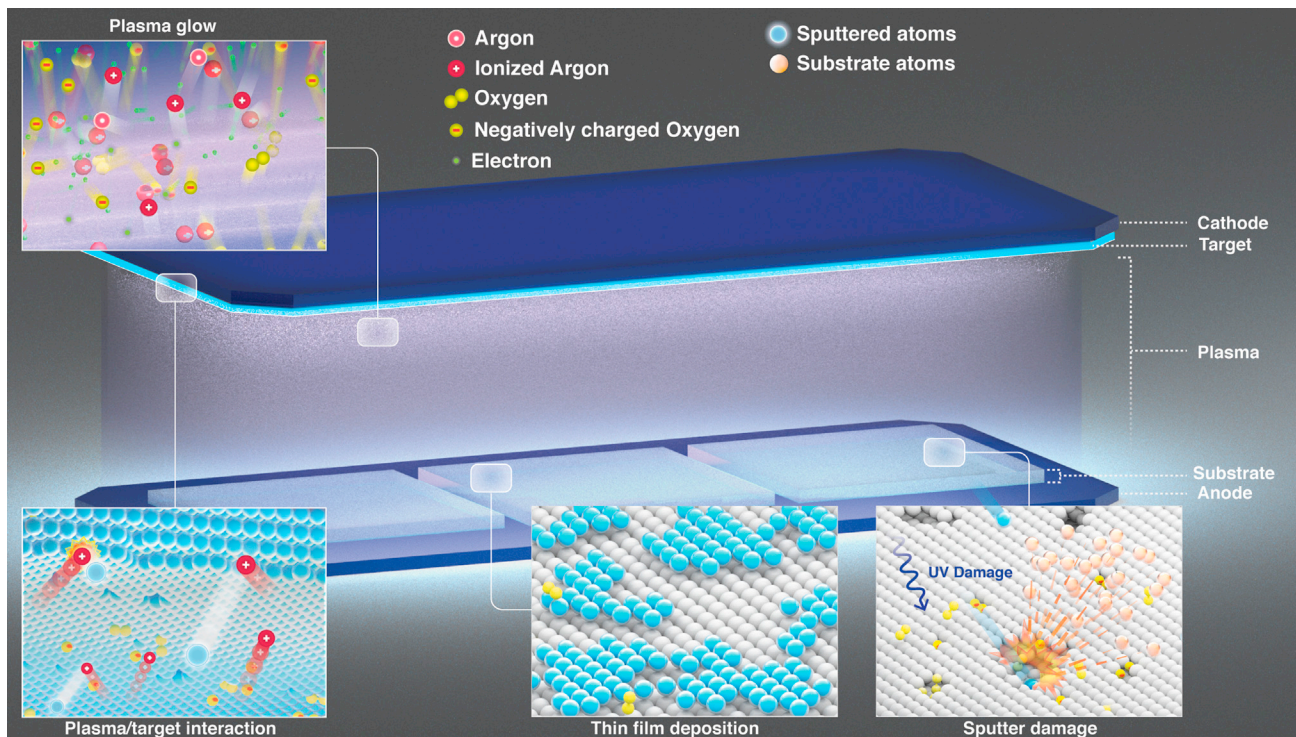


Figure 1. Sputtering process

Illustration of the sputtering process and possible damage mechanisms of the underlying substrate. The sketch explains four main physical phenomena occurring during the sputter deposition of oxide films: i.e., plasma excitation, plasma/target interaction, thin-film deposition, and sputter damage due to ion bombardment.

The discharge voltages during sputtering typically range between -200 and -800 V and will depend on the desired process conditions and specific configuration of the sputtering system. Usually, RF sputtering requires lower discharge voltages than DC sputtering (deposition by both DC and RF plasma excitation is possible for conductive materials, such as TCOs). Notably, the magnitude of the discharge voltage is linked to the level of the sputtering damage, where the application of RF sputtering might help minimize this damage.^{36,38}

Sputter damage during TCO deposition is commonly attributed to the substrate's bombardment by highly energetic species. An elaborate discussion of the influence of ion bombardment on the electrical and structural properties of TCOs is given in a dedicated review by Ellmer and Welzel.³⁴ Here, we provide a nonexhaustive description of the main species involved in the process and the representative energies they can acquire from the following references:^{34,39}

- Sputtered atoms (ions) from the target surface (~ 10 eV), the formation of which mainly depends on the binding energy of the target material;
- Negative ions (originating from the carrier gas) formed in the plasma (~ 5 – 15 eV), the formation of which mainly depends on the plasma potential;
- Negative ions formed at the target surface (up to 400 eV), the formation of which mainly depends on the target voltage;
- Positive ions formed in the plasma (~ 15 eV), the formation of which mainly depends on the potential fall in front of a substrate at floating potential;

- Reflected atoms and neutralized ions from the target surface (20–50 eV), the formation of which mainly depends on the background gas and the mass of the sputtered element.

As seen in the list above, negative ions (e.g., O^- and ln^- for ITO sputtering) formed at the target surface and accelerated toward the substrate acquire the largest energy, which is determined by the potential between target and plasma potentials. Although the flux of the energetic particles is an important parameter, it was reported that high-energy negative O^- ions are additionally the most abundant species in plasma in case of reactive deposition of oxides.^{34,35,40,41} However, energies of other ions/atoms (e.g., Ar^+ , Ar^0 , or ln^0) in the discharge may already be sufficient to dissociate surface bonds or etch soft layers in certain device technologies,^{39,42–46} for example, perovskite films (with Pb and I bonding energies of 2.77 and 1.58 eV, respectively),⁴⁵ organic compounds (with C-C, C-O, C-H, and C=C bonding energies of 3.7, 3.5, 3.4, and 6.2 eV, respectively),⁴³ as well as hydrogen bonded to crystalline silicon surfaces or within an amorphous silicon matrix (bonding energies of 3.25 eV).⁴⁶ In addition, the momentum transfer of high-energy particles from the plasma (Ar, oxygen ions) or sputtered from the target might impinge or even increase the substrate temperature sufficiently to trigger physical (e.g., etching) or thermal degradation of sensitive substrate layers. This can affect the functional properties of underlying charge transport and passivation layers and photoactive absorbers or emitters, eroding device performance. For instance, due to sputter damage, there may be inevitable interfacial consequences such as pinning of the Fermi level, caused by damage-related interface gap states, resulting in the formation of Schottky-barrier impeding carrier transport. Sputter damage can also impair the doping efficiency of materials and the lifetime of excess charge carriers in photoactive materials; in some cases, depending on its extent, such damage can even lead to a reduced shunt resistance.⁴⁷ The following sections discuss these consequences on the behaviors of typical optoelectronic devices.

Impact of sputter damage on optoelectronic devices

Solar cells

Thin-film solar cells can be fabricated in either substrate or superstrate configuration. In the *superstrate* configuration, light enters the device through the glass onto which a TCO is deposited, followed by the other device layers, such as the absorber layer (sandwiched between the ETL and HTL), and back contact (either a metal or another TCO in case of semitransparent devices or tandem solar cells). In the *substrate* configuration, the TCO is deposited onto the top charge-selective layer since light enters the device from the layer-stack side, giving freedom to choose a large variety of substrates such as flexible metal foils. In all cases when the TCO needs to be deposited on top of active device layers, damage may be induced, which must be mitigated.

Since typical state-of-the-art devices feature sensitive layers (see examples in [Figure 2](#)), sputter damage is practically unavoidable, motivating the search for adequate buffer layers (discussed in the section “[buffer layers in optoelectronic devices](#)”) or strategies that can undo the damage. For example, in SHJ solar cells, the intrinsic and doped hydrogenated amorphous silicon (a-Si:H) layers that act as passivating and carrier-selective contacts on c-Si wafers are sensitive to sputter damage.¹⁵ Here, the incurred damage can be annealed away without needing an additional buffer layer, which typically occurs during the final metal curing step. For thin-film solar cells in the substrate configuration, such as those based on $Cu_2ZnSn(S,Se)_4$ (CZTSSe), $Cu(In_xGa_{1-x})Se_2$ (CIGS), and CdTe absorbers, a buffer layer (usually n-type) is crucial not only to form

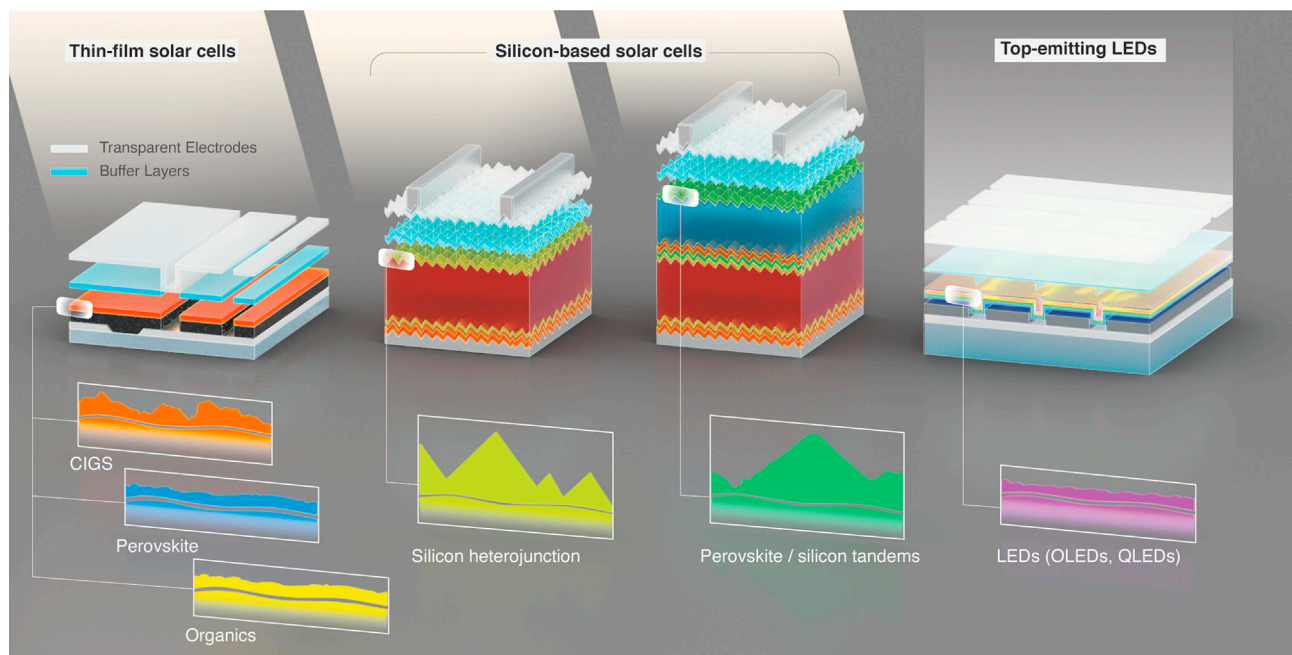


Figure 2. Device sketches of different solar cell technologies and their surface morphologies

Here, transparent electrodes and buffer layers follow the surface morphology of the underlying layers, one of the critical parameters for the deposition method selection of both the buffer layer and transparent electrode.

favorable band alignments, needed for electron extraction,^{48,49} but also to protect the *p*-type absorber from sputter damage. Integrating PSCs in tandem devices such as the perovskite/silicon and perovskite/CIGS implementations has recently become a very active field of research. Such devices, aimed at very high performance photovoltaics, also require the use of TCO layers, often on both sides of the device, as well as in the recombination junction that electrically and optically couples the top and bottom cells (Figure 2).^{50–53}

Suppose solar cells are not protected from sputter damage. In that case, the devices usually show S-shaped current density-voltage (*J*-*V*) characteristics, as shown in Figure 3.^{16,54} Such devices exhibit reduced fill factors (*FF*), open-circuit voltage (*V*_{OC}), and short-circuit current density (*J*_{SC}) values, leading to low maximum power point (MPP) values. However, the observed S-shape often cannot be simply explained by suboptimal series and shunt resistances. For each type of solar cell, the source and the consequences of the damage may vary significantly.

For PSCs involving TCOs sputtered on the device stack, numerical simulations using equivalent circuit models suggest that the main reason for the observed S-shaped *J*-*V* curves is the formation of a Schottky diode at the TCO/HTL interface, where the sputtering process is performed (Figures 3A–3C). For example, in regular, semitransparent *n*-*i*-*p* devices (where the HTL [*p*-layer] is deposited onto the perovskite [*n*]), S-shape curves have been attributed to structural changes in spiro-OMeTAD, which is a widely used HTL, and an increase in the Schottky barrier at the TCO/spiro-OMeTAD interface upon TCO sputtering.¹⁶ If no buffer layer is used, increasing the processing time (Figure 3C) and sputter power (Figure 3D) results in more pronounced S-shaped *J*-*V* curves, and thus lower MPP values.^{12,16} Here, a common mitigation approach is the insertion of evaporated MoO_x (featuring good optical transparency and a high work function) as a buffer layer between the TCO and spiro-OMeTAD.¹² For the inverted *p*-*i*-*n*

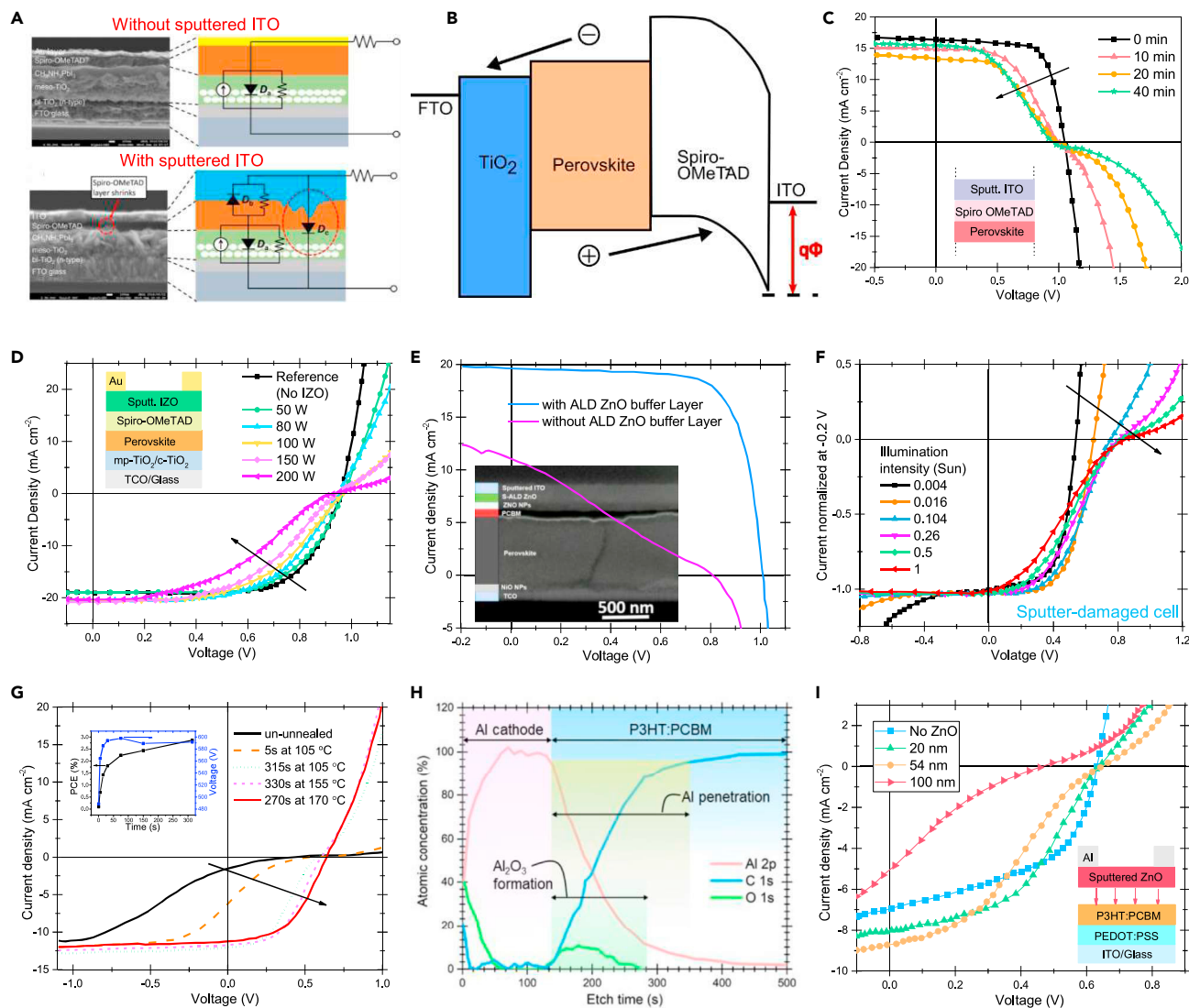


Figure 3. Sputter damage in perovskite and organic solar cells

(A) Cross-sectional scanning electron microscopy images and corresponding schematic representation of equivalent circuit model between layers of PSCs with and without sputtered ITO layer.

(B) Band diagram of corresponding PSCs showing the Schottky junction formed between spiro-OMeTAD and sputtered ITO.

(C) Current density-voltage characteristics for increasing sputtering time of ITO layer in PSCs. The arrow indicates the direction of increasing sputtering time, and the inset shows the corresponding device structure. Reprinted with permission from Kanda et al.¹⁶ Copyright 2016, American Chemical Society.

(D) Current density-voltage curves of *n-i-p* PSCs without buffer layer show the S-shape formation regarding increasing sputtering power of IZO layer deposition. The arrow indicates the direction of increasing sputtering power, and the inset shows the schematic device structure used for measurements. Adapted from Werner et al.¹²

(E) Current density-voltage characteristics of *p-i-n* PSCs with and without a spatially atomic layer deposited ZnO buffer layer. The inset is the SEM image of the corresponding devices. Reprinted with permission from Najafi et al.⁵⁵ Copyright 2018, Wiley-VCH.

(F) The change in current-voltage characteristics with varying illumination intensities from 0.004 to 1 sun (normalized at -0.2 V) for a cell with an IZO layer sputtered at 150 W. The arrow indicates the direction of increasing illumination intensity, and the device structure used for measurements is the same as in (D). Adapted from Werner et al.¹²

(G) Current density-voltage curves of OSCs with sputtered Al contacts for different annealing times and temperatures. The arrow indicates the direction of increasing annealing temperature and time. The insets show the evolution of PCE and V_{OC} compared with annealing time (annealed at 105°C) for devices. Adapted from Ahlswede et al.⁵⁶

Figure 3. Continued

(H) An x-ray photoelectron spectroscopy depth profile of a P3HT:PCBM film covered with 100 nm of aluminum by sputtering with a target power of 1500 W, demonstrating aluminum (pink), carbon (blue), and oxygen (green). Adapted from Griffith et al.⁴⁷

(I) Current density-voltage curves of transparent OSCs without RF magnetron sputtered the ZnO cathode interfacial layer in different thicknesses. The inset shows the device structure used for measurements. Adapted from Jouane et al.⁵⁷

configuration (where now the HTL is deposited before the perovskite), the frequently used ETLs (e.g., C_{60} and derivatives) are also sensitive to sputter damage, again requiring a buffer layer, e.g., ZnO or SnO_x (featuring again good transparency but now a low work function) (Figure 3E).^{55,58} For sputter-damaged devices, temperature-dependent J - V measurements can be useful to identify the formation of a Schottky barrier at the interfaces and quantify the barrier height. Light intensity-based J - V measurements can give hints about the presence of sputter damage, as at higher light intensities, the S-shaped behavior becomes more prominent (Figure 3F).¹² Also, surface-sensitive UV photoelectron spectroscopy (UPS) might provide insight into changes in energy levels due to sputtering damage.

Semiconducting polymers such as poly(3-hexylthiophene) (P3HT) are frequently studied in OSCs, which can also be damaged by metal-electrode sputtering. Indeed, highly energetic metal atoms may break the chemical bonds in the polymer, affecting its conjugation length and reducing the charge mobilities.⁵⁶ Fortunately, this deterioration can be partially recovered by post-annealing (Figure 3G), similar to SHJ solar cells. Nevertheless, metal sputtering on soft organic layers may also result in metallic current paths since highly energetic negative ions can penetrate the layers. For instance, aluminum sputtering on the P3HT:phenyl-C61-butyric acid methyl ester (PCBM) layers without buffer layers results in the penetration of aluminum atoms up to 8 nm into the organic layers and the formation of highly insulating aluminum oxide (Al_2O_x) at the interface between the aluminum electrode and the organic film, especially for higher sputtering powers (Figure 3H).⁴⁷ As another example, sputtering ZnO as a cathode interfacial layer on the photoactive layer of p - i - n OSCs changes the photoactive layer/ZnO interface morphology, which results in a high Schottky barrier and consequently in S-shaped J - V curves (Figure 3I).⁵⁷ Such damage can be irreversible. Due to the reasons mentioned above, sputtered top electrodes have not yet been fully explored in OSCs; instead, thermally evaporated thin metallic films are frequently used as transparent top electrodes. Nevertheless, the recent advances in the power conversion efficiency (PCE) of semitransparent OSCs (having increased to 12%) has been achieved at the cost of low average visible light transmittance (~19%), urging for the development of better transparent electrodes.⁵⁹

As already alluded to, in SHJ solar cells, degradation of the a-Si:H/c-Si interface is commonly observed after the TCO deposition (Figures 4A–4C).^{15,60} This process might be critical also for perovskite/silicon tandem solar cells since the recombination layer and charge-selective contact depositions required for the bottom contact of the perovskite top cell might necessitate a sputtering process on top of the SHJ bottom cell.⁶¹ The damage, as evidenced by a loss in surface passivation quality of the SHJ cell, is a result of the formation of Si dangling bonds at the a-Si:H/c-Si interface.¹⁵ Fortunately, this degradation can be recovered by annealing, as stated, usually during metal-paste curing of the grid electrode of the devices (Figure 4B). The cause of the damage is at least in part from plasma emission, as evidenced by employing samples covered by glass or quartz during the sputtering process, resulting in a persistent decrease in passivation quality (Figures 4A and 4C). Such sputter damage to the contact-layer/absorber interface has also been shown to adversely impact the FF , mainly due to the decrease in excess charge carrier lifetime at the

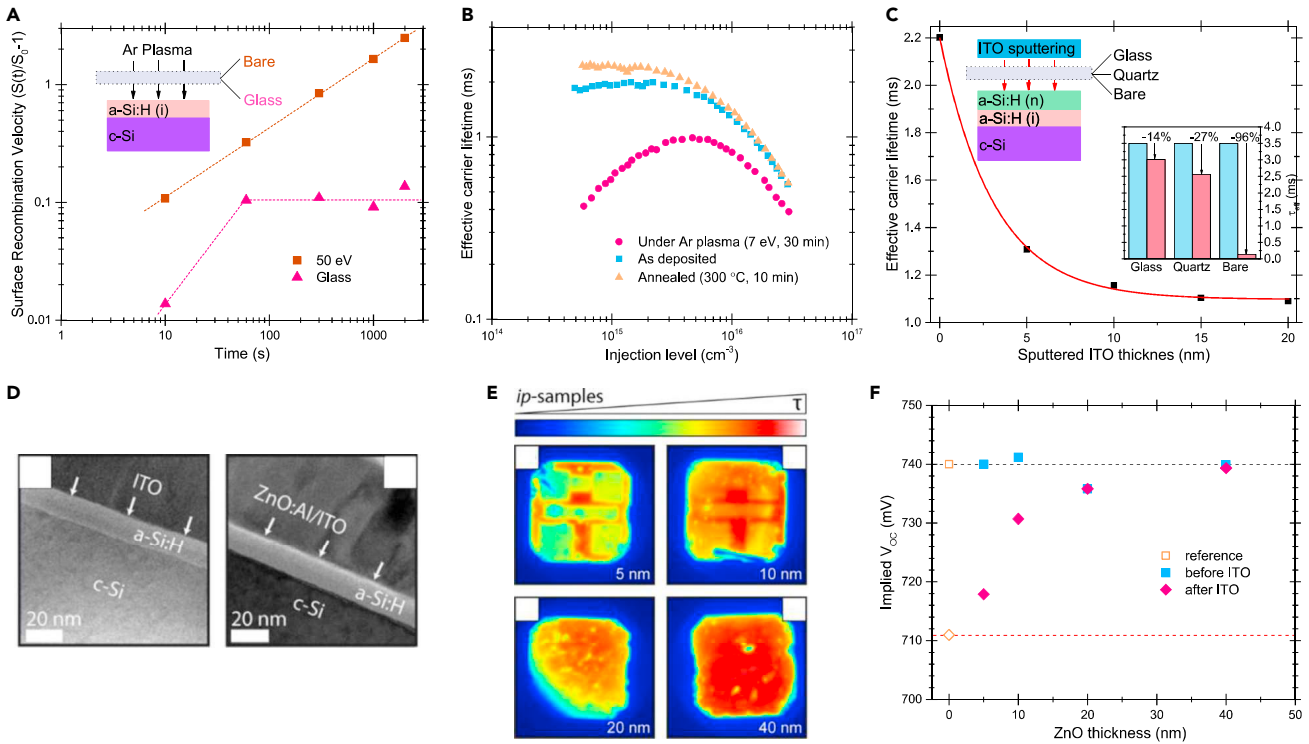


Figure 4. Sputtering damage and buffer layers in silicon heterojunction solar cells

(A) Variation in the value of surface recombination velocity for a-Si:H passivated c-Si wafers covered by the glass while exposed to Ar plasma, without any external biasing, and biased with a voltage of -50 eV without glass. The inset shows the schematic cell structure and Ar plasma application with or without glass protection.

(B) The change in effective carrier lifetime value for as-deposited a-Si:H film on c-Si wafers after Ar ion bombardment and thermal annealing. Adapted from Illiberi et al.⁶⁰

(C) The variation of effective carrier lifetime of an n-type wafer with a-Si:H layers measured as a function of sputtered ITO thickness with corresponding device architecture used in measurements. The insets demonstrate the device architecture used in measurements and effective carrier lifetime of a wafer passivated with a-Si:H in the as-deposited state and after sputtering both when left bare and when protected by glass or quartz (the percentages indicate relative losses in a lifetime). Adapted from Demareux et al.¹⁵

(D) Transmission electron microscopy images of silicon heterojunction solar cells without and with atomic layer deposited Al-doped ZnO (5 nm) buffer layers.

(E) Photoluminescence images of cells (shown in D) after ITO deposition by sputtering with varying thicknesses of the atomic layer deposited Al-doped ZnO from 5 to 40 nm.

(F) The change in implied V_{OC} values before and after ITO deposition for the samples shown in (D). The black and red dashed lines depict the value of devices before and after ITO deposition without atomic layer deposited Al-doped ZnO (the orange open-data points). Reprinted with permission from Demareux et al.⁶³ Copyright 2014, IEEE.

MPP (i.e., via injection-dependent recombination), but possible also because of interfacial Fermi-level pinning effects, inducing Schottky barriers. Despite the fact that post-annealing can recover most, if not all, of the interface passivation electronically, infrared spectroscopy indicates that the a-Si:H contact layers can be structurally permanently damaged following overlayer sputtering.¹⁵ It may thus be beneficial to insert a buffer layer to avoid such damage. Implementing thin atomic layer deposition (ALD) ZnO films in between the sputtered TCO and a-Si:H stacks may serve that function (see Figures 4D–4F), even though it was found these layers may act as a resistive interlayer, undesirably increasing the contact resistance, and thus mandating further process optimization.^{62,63}

Similarly, for Cu(In, Ga)Se₂ devices, direct sputtering of TCOs onto CIGS absorbers results in a high resistance at their interfaces, as quantified by the constant phase element (CPE, which is a capacitance-like element) measured via impedance

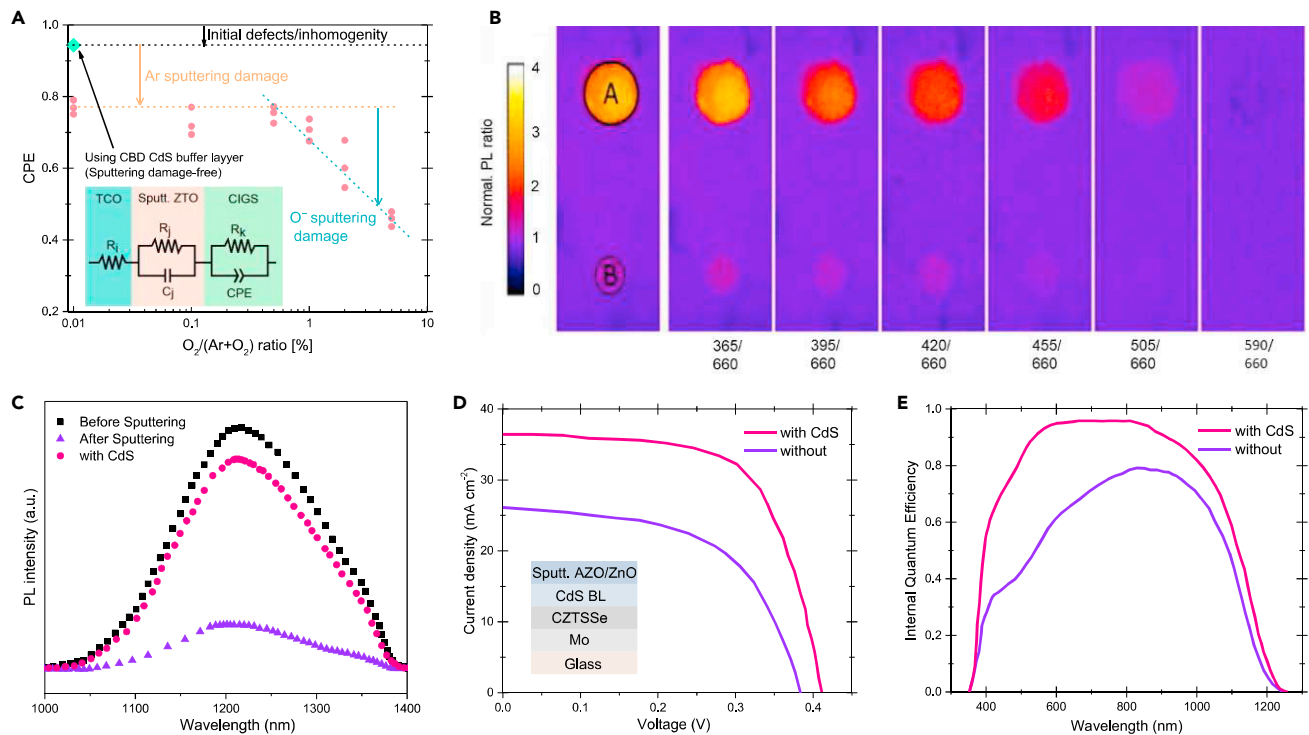


Figure 5. Sputtering damage and buffer layers in CZTSSe and CIGS solar cells

(A) Constant phase element of CIGS solar cells as a function of the oxygen partial pressure during RF sputtering of the ZTO layer. The inset shows the proposed equivalent circuit model of the CIGS solar cells for impedance spectroscopy measurement. Adapted from Sugiyama et al.⁶⁴

(B) Normalized photoluminescence intensity ratio images in different excitation wavelengths for a CdS/CIGS/Mo sample. The A and B display intentionally thinned down zones of the CdS layer by acidic etching. The ratio images are normalized using the un-etched part of the sample as a reference. Reprinted with permission from Rey et al.⁶⁵ Copyright 2020, IEEE.

(C) Photoluminescence intensity of CZTSSe devices with and without CdS buffer layer before and after AZO/ZnO sputtering.

(D) Current density-voltage characteristics for devices with and without CdS buffer layer upon AZO/ZnO sputtering. The inset depicts the device structure employed for measurements in (C) to (E).

(E) Internal quantum efficiency curves of CZTSSe devices with and without CdS buffer layer upon AZO/ZnO sputtering. Adapted from Matsuo et al.⁴⁸

spectroscopy (Figure 5A).⁶⁴ With increasing oxygen partial pressure in the sputtering process, thereby increasing the density of plasma species, the CPE diverges substantially from the ideal case ($CPE = 1$), indicating the formation of trap-state defects at the related interface hampers charge transport at the top contact. Photoluminescence (PL) intensity maps of the CdS/CIGS/Mo (top to down) for various thicknesses of the cadmium sulfide (CdS) layer show that specific thicknesses are needed for adequate protection (Figure 5B), which is discussed in detail in the section “buffer layers in optoelectronic devices.”⁶⁵ As for the other types of thin-film solar cells, sputter damage usually causes quenching of the PL signal, and the device performance is deteriorated, as exemplified for CZTSSe films in Figures 5C and 5D.^{48,66} This damage is usually attributed mainly to bulk defects and disorder and is responsible for a high V_{OC} deficit ($E_g/q - V_{OC}$, where E_g is the bandgap of the material and q is the electron charge) of the devices.⁶⁷

Generally, monitoring the level of the damage is important. For this, several alternative techniques to those already mentioned can be considered, such as illuminated lock-in thermography and forward- and reverse-bias dark lock-in thermography techniques for probing the breakdown sites where current flows through weak diodes, shunts, and defects.⁶⁸ Fast determination of the carrier lifetime for perovskite absorbers is challenging due to the shorter carrier lifetimes of the perovskite films

(within nanosecond scales, resulting from its direct bandgap nature) compared with crystalline silicon (up millisecond scale, resulting from its indirect bandgap nature), thereby necessitating the use of time-resolved PL measurements, which usually take several hours.⁶⁹ Meanwhile, steady-state PL can be used for fast monitoring of the sputtering damage, as damaged layers show reduced PL peak intensity, as discussed above. Also, for large-area imaging, hyperspectral luminescence imaging can give quantifiable outputs for the carrier recombination induced by defects via the contrast on the PL or EL signal counts.⁷⁰ In addition, X-ray photoelectron spectroscopy (XPS) can be a versatile tool to monitor the chemical and electronic changes in soft layers underneath the sputtered TCOs or the sputtered TCOs themselves.^{71,72} XPS helps to observe the broken chemical bonds of the organic layers upon Ar irradiation,⁷³ Ar implantation from sputter gas into the growing film,⁷⁴ formations of additional layers at the interface of organic films/sputtered TCOs at high sputtering powers.⁷⁵ Also, utilizing the UPS, changes in Fermi level at the substrate surface due to the oxygen implantation from the plasma were detected,⁷⁴ showing the undesired outcomes of sputtering. All these techniques provide detailed information about the sputtering damage on the layers, whereas *J-V* scans can give information about the overall device behavior. These techniques are well-established for conventional solar cell development and could be adopted by the PSC and OSC communities for faster diagnosis of process-induced damage and feedback for device development.

Light-emitting diodes

Top-emitting and transparent LEDs are essential for making active-matrix displays having high-resolution and see-through displays. Standard OLEDs are mostly vacuum-processed, usually in the *n-i-p* configuration in which light is emitted from the electron-injecting (*n*) contact. Thus, the implementation of TCOs (that have work functions >4 eV) as top electrodes in transparent OLEDs (the same in QLEDs) requires the use of low work function buffer layers (preferably vapor deposited) at the TCO/organic interface for efficient injection of electrons into the device at relatively low operational voltages.

OLEDs with sputtered metal electrodes show an undesired high leakage current in their *J-V* curves (Figure 6A), and degradation of underlying materials by sputtering is evident, as demonstrated by optical and scanning electron microscope (SEM) images in Figure 6B.⁷⁶ As discussed above, PL quenching tests are helpful for solar cells, eliminating the need for complete device fabrication to make the appropriate diagnosis. A systematic experiment using this strategy, such as exposing the aluminum (III) bis(2-methyl-8-quinolinato)-4-phenylphenolate (BALq) respectively to an Ar ion beam (AIB), oxygen ion beam (OIB), electron beam (EB), and UV light, has revealed that the oxygen ions from the sputtering plasma are the root cause of the sputter damage.⁷⁷ The damage caused by the oxygen species is evident from the PL intensity of BALq films after exposure to an oxygen plasma. From quenched PL values of BALq₃ films, the magnitude of the damage can be ordered as UV < electrons < Ar ions < oxygen ions, as shown in Figure 6C. Increasing the sputtering power will increase the energy carried by the particles and cause more damage to soft layers (Figure 6D). Then, the damage level is also scaled with longer processing times. Excessive damage can lead to completely shorted devices, especially when the soft underlayers are very thin, either via particles with high kinetic energy or the long exposure time.

Also, organic tris(8-hydroxyquinoline)aluminum(III), Alq₃ (an electron-transport and emitting material widely used in LEDs) irradiated with 100 eV Ar⁺ ions from a UV

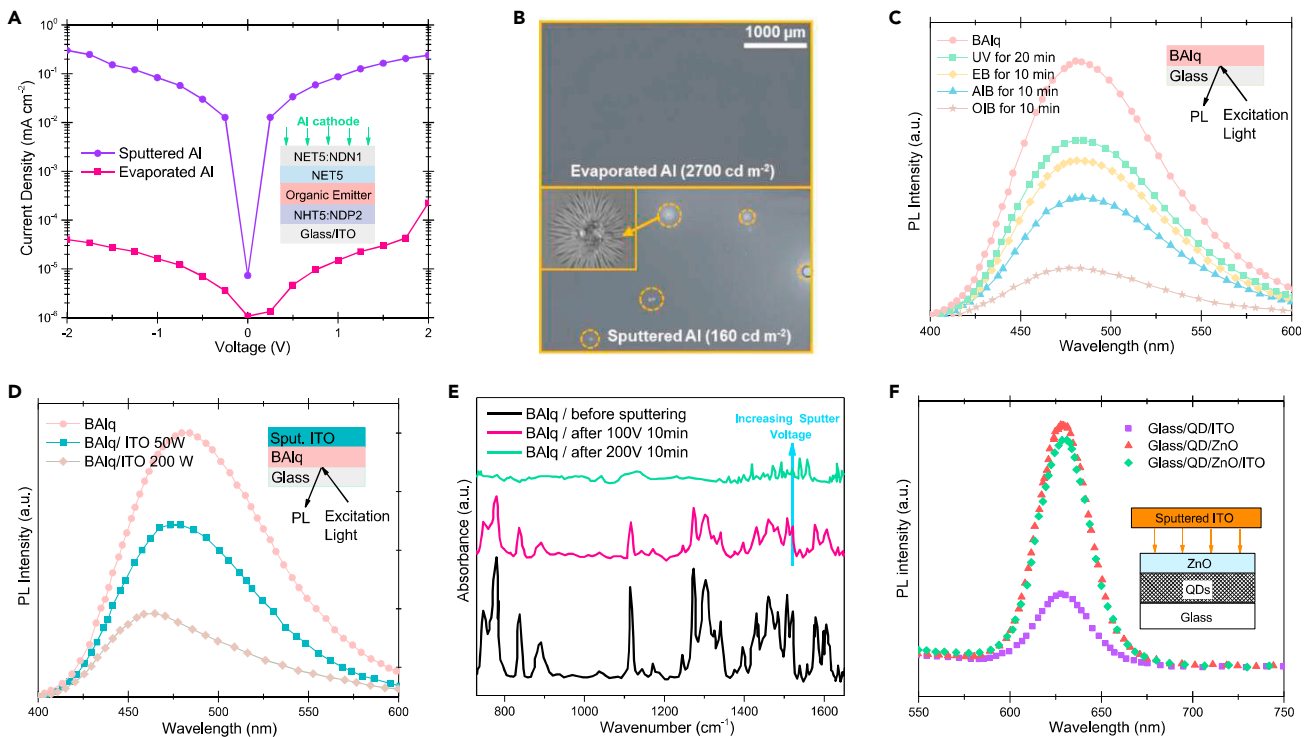


Figure 6. Sputtering damage in LEDs

(A) Current density-voltage curve of OLEDs with evaporated and sputtered Al cathodes showing the increased leakage current upon Al sputtering. The inset represents the corresponding device structure.

(B) Optical images of OLED surfaces having evaporated (luminance: $2,700 \text{ cd m}^{-2}$) and sputtered (luminance: 160 cd m^{-2}) Al cathodes after operation at 3 V. The inset in the optical image of a sputtered Al cathode is an SEM image of bright spots showing the degradation of sputtered Al after current-voltage-luminance measurement. Reprinted with permission from Gil et al.⁷⁶ Copyright 2009, Elsevier Inc.

(C) Photoluminescence spectra of BAQ organic film after AIB, OIB, and EB bombardment, and UV radiation. Adapted from Lei et al.⁷⁷

(D) Photoluminescence spectra of BAQ film before and after ITO sputtering with increasing operation power. Adapted from Lei et al.⁷⁸

(E) Fourier transform infrared spectroscopy of BAQ organic layers before and after oxygen ion bombardment at different voltages (100 V and 200 V). Adapted from Lei et al.⁷⁷

(F) Photoluminescence spectra of colloidal CdSe/CdS/ZnS QDs with and without sputtered ITO and ZnO buffer layer. The inset depicts the device configuration used for measurements. Adapted from Wang et al.⁷⁹

beam, shows broken bonds of Alq_3 (N-Al, C-O-Al) as revealed from peak broadening of XPS spectra and shifting in the core spectra of Al, O, N, and C.⁷³ For transport layers like BAQ, a very similar compound to Alq_3 , the peak intensity reduction of the Fourier transform infrared spectroscopy (FT-IR) spectra after oxygen ion bombardments can also give an idea for the level of the induced damage. Figure 6E shows that oxygen ions with high energy not only induce considerable damage but also may cause a chemical reaction between oxygen ions and the BAQ film.⁷⁷ Similar to OLEDs, QLEDs are highly sensitive to sputter damage, necessitating the use of buffer layers, as depicted in Figure 6F.^{79,80} CdSe/CdS/ZnS QD films exhibit relatively weak PL response under ITO sputtering, which verifies the induced damage; however, using a ZnO buffer layer alleviates the effects of the sputtering process.⁷⁹

BUFFER LAYERS IN OPTOELECTRONIC DEVICES

To fully utilize the merits of the sputtered TCOs, implementing an additional protection layer is the state-of-the-art solution to prevent the formation or mitigate the extent of sputter damage for various optoelectronic devices (as sketched in Figure 2). Regardless of the device application, a suitable buffer layer should satisfy the

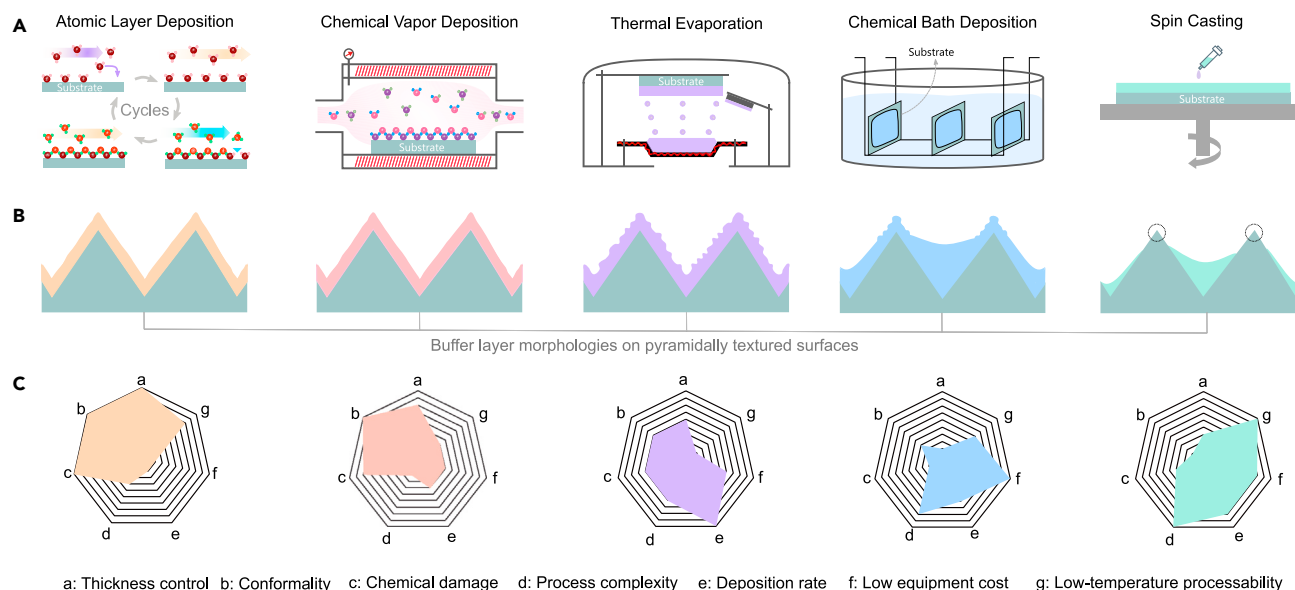


Figure 7. Various buffer-layer deposition techniques

(A) Sketches of the commonly used buffer-layer deposition techniques.

(B) Morphologies on pyramidal textured silicon surfaces of different deposition technologies. Here the textured surfaces are chosen as the representative of the most complex surfaces.

(C) The direct comparison of the deposition techniques with a spider chart.

following criteria: (1) well-matched energy alignment with the adjacent materials for efficient charge transport, (2) wide bandgap for high optical transmission, (3) an excellent refractive index match with the adjacent transparent electrode for minimized reflection (this can be verified by optical simulations),^{26,81} (4) chemical inertness against underlying materials, (5) high uniformity and density of thin films (typically 5–60 nm), (6) act as a diffusion barrier to prevent migration of cations and penetration of moisture, (7) low-temperature (preferably <100°C for most of the semiconductors) and damage-free deposition, and (8) resilience to sputtering of subsequent layers. These requirements limit the materials choice and deposition techniques for the buffer layers (Figures 7A and 7B), as we summarized in the pros/cons of various deposition techniques in Figure 7C.

To compare deposition technologies' compatibility with buffer layers, we calculated figures of merit (FOMs) for each method. To do this, we first scaled each asset from 1 to 5 and visualized them in the spider chart (Figure 7C), where every two heptagons correspond to 1, and the last heptagon corresponds to 5 in scale. ALD is the slowest process among the deposition methods, and growing layers takes a long time; therefore, we considered it as 1, layers can be produced quickly in thermal evaporation (TE); we scored it as 5. In terms of low equipment cost, chemical bath deposition (CBD) is the cheapest one (1) such that one may need only a hot plate, magnetic stirrer, and container, whereas ALD (5) and chemical vapor deposition (CVD) (4) machines/apparatus are highly expensive. When it comes to processing complexity, spin-coating took the highest value (5) since pH, concentration, and temperature of solution and speed of rotation can significantly affect the nucleation and growth process and hence stoichiometry and quality of final layers, whereas CVD (1) and ALD (2) are vacuum-based methods, so controlling the growth process is relatively easy. According to these considerations, FOMs for each deposition method were calculated as follows:

$$\text{FOM} = \frac{\text{Sum of scaled positive factors}}{\text{Sum of scaled negative factors}} \quad (\text{Equation 1})$$

in which positive factors are thickness control, conformality, deposition rate, low equipment cost, and low-temperature processability, while chemical damage and process complexity are negative ones. We found FOMs of CVD, CBD, TE, ALD, and spin-coating of the buffer layers as 3, 2.8, 2.5, 2.3, and 2.3, respectively. Even though the ALD and TE have extensively been employed to fabricate buffer layers, they demonstrated relatively low FOMs stemming from the equipment cost, which is an external factor that largely affects the calculation. The following subsections provide a more elaborate discussion on the previously reported buffer layers for solar cells and LEDs with various growth techniques with a cross-field learning perspective.

Solution-processing techniques

Solution-processing techniques are usually a primary choice for thin-film deposition due to their simplicity and low capital cost. Hence, not surprisingly, solution-processed buffer layers are frequently reported in the literature. For instance, presynthesized metal-oxide nanocrystals can be deposited as buffer layers via spin-casting, spray, or blade coating if the suspensions can be achieved in low-polarity solvents (since high-polarity solvents may damage underlying sensitive layers such as perovskite films or organic charge transport layers). Since these materials are presynthesized, preparing suspensions with low boiling point solvents (such as ethanol, isopropanol, etc.) allows for low-temperature processing (nevertheless, usually, a <100°C annealing step is needed to evaporate the solvent).⁸² These advantages make this approach a suitable “soft” deposition technique for buffer-layer processing since the underlying sensitive layers can be kept undamaged. Here, the primary concern can be the chemical damage on the underlying layers with solvent interaction, which, as mentioned, can be mitigated by selecting an appropriate low-polarity solvent, if possible.

In the spin-casting technique, the thickness of buffer layers mainly relies on the rotation speed (in the case of spin casting) and the solution concentration. The uniformity and complete coverage (on flat substrates) can be ensured by controlling the size of nanoparticles and the surface roughness of the underlying layers. In this sense, ZnO (Figure 8A),^{13,79,83} SnO_x (Figures 8B and 8C),⁸⁴ AZO,¹¹ ITO,⁸⁵ and WO_x⁸⁶ nanoparticles (average particle size is 15–100 nm, as exemplified with transmission electron microscopy images in Figure 8B) have been reported as buffer layers to protect the organic layers of PSCs, OSCs, and QLEDs. In addition, to protect against sputtering damage, SnO₂ nanoparticle-based thin films also exhibited good environmental stability under high humidity conditions when employed as a buffer layer in PSCs, as displayed in Figure 8C. In transparent QLEDs, ZnO nanoparticles and a blend of ZnMgO nanoparticles and polyvinylpyrrolidone have been utilized as a buffer layer.^{87,88} Meanwhile, the library for metal-oxide nanoparticles is quite rich. For instance, Nb₂O_x, V₂O_x, NiO, and MgO nanoparticle-based thin films have been well documented for various applications.⁸⁹ Yet, these solution-processed nanoparticle thin films have yet to be utilized as buffer layers and deserve to be examined. Notably, the main disadvantage of spin-coating in this context (besides possible throughput and ineffective materials usage issues) is the incapability to deposit an ultrathin layer (<5 nm) since metal-oxide nanoparticles need a certain thickness to form a continuous film.⁹⁰ Solution-processed polyelectrolytes can also act as a buffer layer due to their high mechanical stability originating from long-chain structures. For instance, polyethyleneimine ethoxylated (PEIE) protects the sensitive C₆₀ layer from sputter damage (Figures 8D and 8E). Its application to two-terminal (2T)

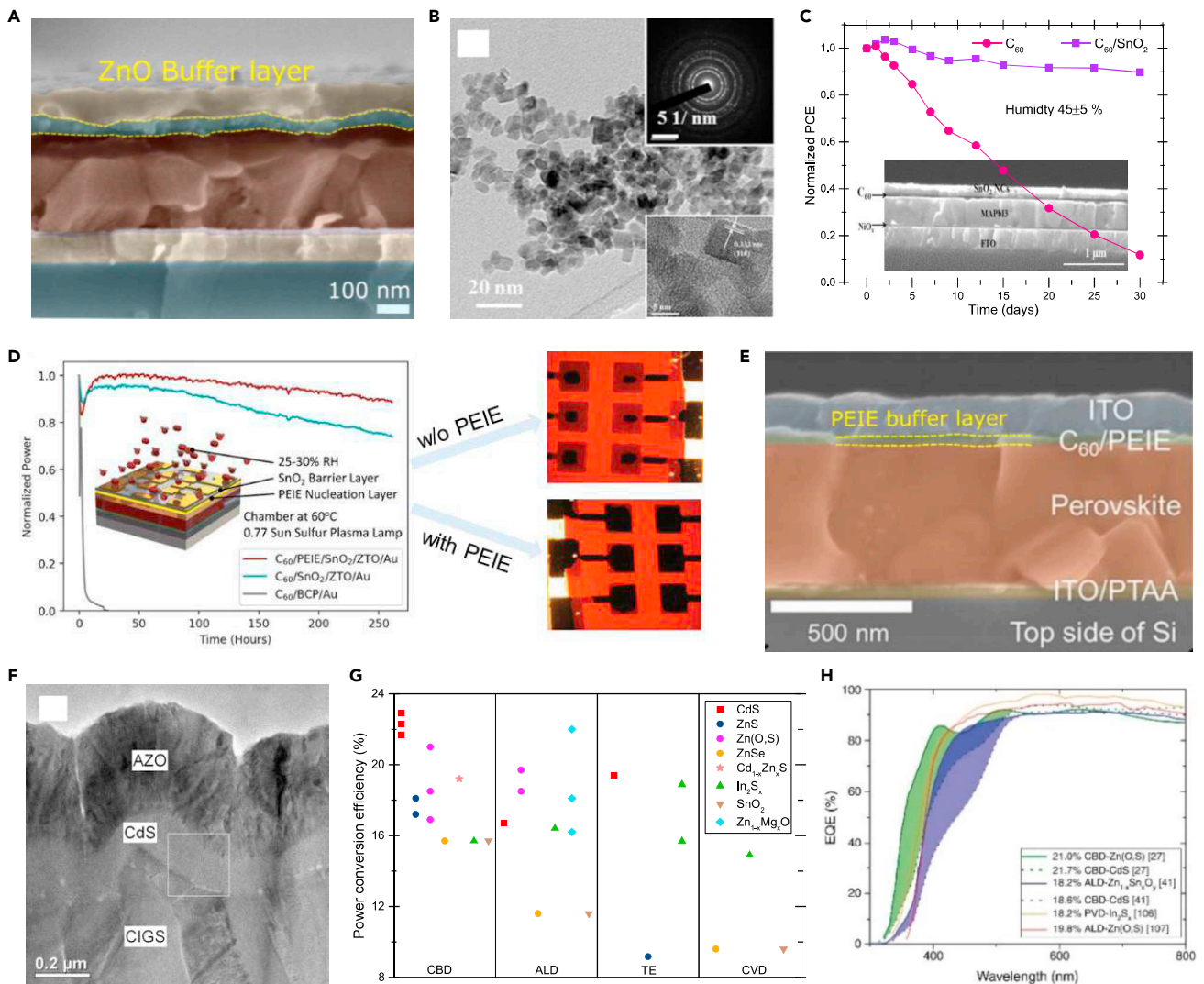


Figure 8. Solution-processed buffer layers for optoelectronic devices

(A) Cross-sectional SEM image of a *p-i-n* perovskite solar cell with solution-processed ZnO buffer layer. Reprinted with permission from Aydin et al.¹³ Copyright 2019, Wiley-VCH.

(B) Bright-field transmission electron microscopy images of SnO₂ nanoparticle solution. Upper and bottom insets are corresponding diffraction patterns and high-resolution transmission electron microscopy images, respectively.

(C) Stability test of *p-i-n* PSCs with and without spin-coated SnO₂ buffer layer. The inset shows the SEM image of corresponding devices. Reprinted with permission from Zhu et al.⁸⁴ Copyright 2016, Wiley-VCH.

(D) Stability test results of unencapsulated PSCs with and without PEIE nucleation layers. Inset shows the device architecture and test conditions. Photographs of unencapsulated devices with and without PEIE layer after stability test done under N₂ environment and at 85°C over 670 h. Black regions show the remaining perovskite film after the stability test, and lighter regions on the metal pixels are correspond to areas where the Ag contact corroded due to halide diffusing. Reprinted with permission from Raiford et al.⁹⁴ Copyright 2019, Wiley-VCH.

(E) Cross-sectional SEM image of a *p-i-n* perovskite solar cell with solution-processed PEIE buffer layer between C₆₀ and sputtered ITO. Reprinted with permission from Kim et al.⁹¹ Copyright 2020, American Association for the Advancement of Science.

(F) Cross-sectional transmission electron microscopy image of sputtered AZO/chemical bath deposited CdS/CIGS structure. Reprinted with permission from Han et al.⁹⁵ Copyright 2014, Elsevier Inc.

(G) PCE values of CIGS devices with various buffer layers fabricated by different methods. Data are taken from Naghavi et al.,⁹⁶ Mughal et al.,⁹⁷ Gour et al.,⁹⁸ and Nakamura et al.⁹⁹

(H) External quantum efficiency curves for CIGS cells with different buffer materials deposited by various methods. All cells include anti-reflection coatings, and shaded areas below the curves indicate the current gain relative to the corresponding CdS reference when available. Reprinted with permission from Feurer et al.¹⁰⁰ Copyright 2016, Wiley-VCH.

monolithic perovskite/silicon tandem solar cells resulted in a PCE of 26.7% with 76.4% certified *FF* (see Figure 8E for cross-sectional SEM image of the device).⁹¹ These results show the equivalent performance of the PEIE layers as a buffer layer; however, how this layer prevents the sputter damage is still unclear, although electronically, it is known to act as a work function modifier of the TCOs.^{92,93} Adapting the spin-casting technique to micron-scale rough surfaces, such as random pyramid textured crystalline silicon solar cells for tandem applications, is impractical (see Figure 7).^{11,85} For such rough surfaces, spray coating can circumvent the limitations of the spin-coating technique and may therefore be suitable for scaling up the processing of such materials. However, no successful example has been reported for spray-coated buffer layers on large, textured substrates. Further research in this direction is required for definitive successful demonstrations on large, industrially applicable areas.

CBD, another solution-based technique, involves forming ionic species in a bath solution, followed by transport and condensation of these species on the substrate. The thickness, homogeneity, and density of the CBD-deposited films are linked with the choice of the solution (alkaline or acidic), composition and temperature of the solution, deposition time, and the substrate's surface properties.¹⁰¹ In this case, cadmium sulfide (CdS)^{102,103} (Figure 8F) and zinc sulfide (ZnS)^{104,105} have been commonly used CBD-grown buffer layers enabling high and reproducible efficiencies of chalcopyrite and CdTe thin film solar cells. Meanwhile, the search for alternative CBD buffer layers is ongoing, with Zn(S, O), Cd_{1-x}Zn_xO, In₂S₃, and SnO_x as possible options. For CBD buffer-layer formation, the device stack is immersed into the bath and is subjected to advantageous chemical etching for removing oxides and other impurities of the device-exposed layer surface (for instance, CIGS or CdTe layer surfaces).⁹⁶ CBD-grown buffer layers established high-efficiency CIGS solar cells at low deposition temperature. However, this technique is not favorable on top of the perovskite and organic-based devices since the substrate is immersed primarily in an aqueous solution, likely leading to the dissolution of the underlying layers.¹⁰⁶ Also, the long waiting time (usually >10 min to hours) to reach the thickness of the required film is another drawback of the technique.²⁹

Thermal evaporation

Surfaces that have rough features, such as random pyramidal textured silicon, 3D nanostructures, or large roughness depth to width ratio, usually require conformal coated buffer layers. Here, conformality signifies a film with a nearly constant thickness perpendicular to its underlying substrate surface. Nonconformal buffer layers typically do not provide sufficient protection in the thinner areas, whereas in thicker areas they may cause series resistance. Therefore, for such complex surfaces, vacuum-based thin-film deposition techniques are usually the first choice for several classes of materials. Its low particle energy (typically 0.3 eV or less)¹⁰⁷ and a high uniformity over a large area make TE a preferable “soft” technique for buffer-layer deposition for many optoelectronic devices.

Thermally evaporated metallic thin films, namely Ag,¹⁰⁸ Mg:Ag,¹⁰⁹ and bilayer of LiF/Al,¹¹⁰ can be used as a buffer layer, as well as a semitransparent electrode, depending on the application. The initial development of top-emitting LEDs involved thin Mg:Ag layers on top of the emissive Alq₃ films.¹¹¹ While ~7.5-nm thin films were reported to be sufficient to prevent sputter damage, they led to elevated required operating voltages in the device. This was attributed to an almost complete oxidation of the Mg film during sputter deposition of ITO and incomplete coverage or

island-like formation of Mg:Ag films on the surface of the Alq₃ layer.¹⁰⁹ The use of relatively thicker (~10 nm) Mg:Ag buffer layers circumvented the problem mentioned above. However, the resultant top ITO electrode exhibited reduced transparency. The main drawback of evaporated metal buffer layers is forming island-like metal domains rather than continuous thin films, which might provide only limited protection from subsequent sputtering. Moreover, evaporated metal buffer layers have low optical transparency.¹¹² One of the strategies to improve film coverage is surface treatments or use of adhesion layers, e.g., depositing an ultrathin (1 nm) layer of Cr between the HTL and Au electrode.¹¹³

One can expect that SnO_x, ZnO, NiO_x, and CuO_x, as *n*- and *p*-type oxides, respectively, can be good candidates as thermally evaporated buffer layers. However, usually, these materials do not melt or sublime effectively, resulting in flawed films. E-beam evaporation is a more effective fabrication method for such materials, but the resulting X-ray radiation produced by the EB (also referred to as *bremstrahlung*) might damage the substrate.¹¹⁴ So far, transition metal oxides, such as MoO_x, V₂O_x, and WO_x, are the most successful examples of thermally evaporated buffer layers.^{12,115–119} Their high work function values give them the character of *p*-type, electron-blocking materials in solar cells and LEDs.^{118,120,121} For fabricating top-emitting or transparent OLEDs, moderately thick metal oxides such as MoO_x¹²² and WO_x¹²³ are frequently incorporated as buffer layers due to their relatively high transparency, the visible region, and their simple thermal evaporation-based deposition. Similarly, the insertion of evaporated MoO_x and V₂O_x buffer layers between the photoactive QD layer and metal electrode in opaque QDSCs enables environmental protection by blocking oxygen and water diffusion and reduces the Schottky barrier height at the contact interface. This leads to enhanced hole extraction, resulting in improved device performances.^{124,125}

From an optical perspective, the moderate bandgap of V₂O_x (2.1 eV), which leads to strong parasitic absorption in the blue part of the solar spectrum, makes it less attractive for application at the sun-facing side in solar cell applications when compared with MoO_x (3.1 eV) and WO_x (3.3 eV) (Figure 9A).¹²⁶ Also, oxygen vacancies generate positively charged structural defect states that act as localized color centers, leading to absorption in the visible (VIS, 400–700 nm) and near-infrared (NIR, 700–1100 nm) parts of the spectrum, depending on their oxidation states.¹²⁶ Notably, the widely used MoO_x buffer layer can suffer from the same issue.¹²⁷ Using such buffer layers requires careful thickness optimization to achieve continuous films, which may come with the cost of increased parasitic absorption. For instance, optimal performance of OLEDs with WO_x have been achieved with 60-nm-thick films (Figure 9B); thinner films suffered from low surface coverage, whereas thicker films led to increased parasitic absorption.¹²³

From a stability perspective, MoO_x can be a source of degradation in devices. For instance, the iodine released from the perovskite layer can react with MoO_x, leading to iodine-deficient surfaces.¹³¹ Considering the higher standard reduction potential of WO₃ (−0.09 E°/V) than MoO₃ (+0.075 E°/V) makes WO₃ a better candidate in terms of stability.¹²⁶ In addition, MgO_x (>4.5 eV) and CrO_x (~3.4 eV) feature high bandgap values and can be thermally evaporated, which make them suitable future candidates to replace MoO_x buffer layers underneath sputtered TCOs.^{132,133} Nevertheless, inserting a thin layer of wide bandgap conjugated molecules with free lone pairs such as 2,2',2''-(1,3,5-benzinetriyl)-tris(1-phenyl-1-H-benzimidazole) (TPBi) or bathocuproine (BCP) between MoO₃ and the HTL (Figure 9C) can prevent the

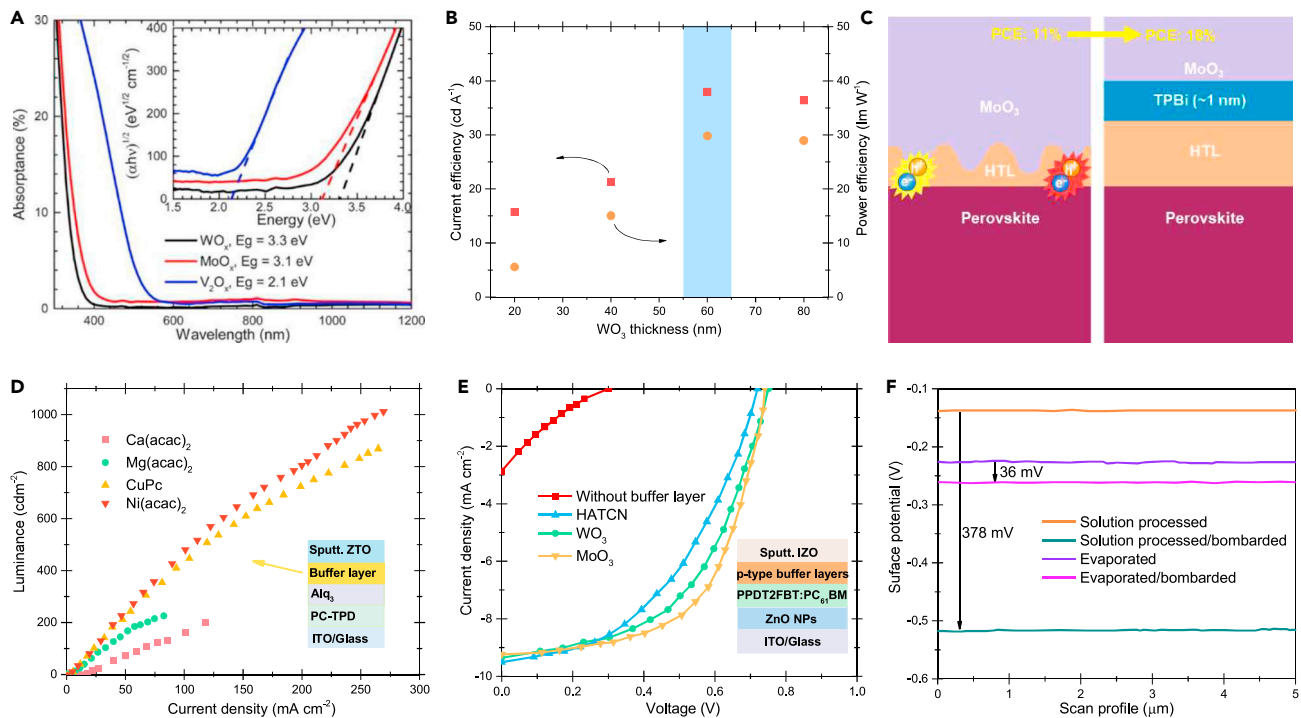


Figure 9. Thermally evaporated buffer layers in optoelectronic devices

(A) Absorbance spectra of widely used hole-selective inorganic buffer layers (in ~ 10 -nm-thick evaporated MoO_x , WO_x , and VO_x layers on glass). The inset is Tauc plots of corresponding buffer layers depicting their bandgaps. Reprinted with permission from Werner et al.¹²⁶ Copyright 2016, American Chemical Society.

(B) Current and power efficiency of transparent OLEDs with respect to varying thickness of WO_3 buffer layer plotted at 100 cd m^{-2} . The aqua area around 60 nm WO_3 indicates the optimum buffer-layer thickness. Reprinted with permission from Meyer et al.¹²³ Copyright 2008, Wiley-VCH.

(C) The schematic illustrates influence of the insertion of TPBi organic film between HTL (spiro-OMeTAD) and evaporated MoO_3 buffer layer in PSCs. Adapted from Perez-del-Rey et al.¹²⁸

(D) Luminescence–current density characteristics of transparent OLED devices with evaporated metal acetate buffer layers. The inset depicts device structure employed for measurements. Adapted from Yamamori et al.¹²⁹

(E) Current density–voltage curves of semitransparent OSCs using various p-type buffer layers. The inset shows device structure used for measurements. Adapted from Kuwano et al.⁸⁶

(F) The variation in surface potential profiles of solution-processed BCP (on PCBM) and evaporated BCP (on C_{60}) buffer layer before and after IZO bombardment. Adapted from Ying et al.¹³⁰

diffusion of MoO_x into the underlying layer and can extend the stability and performance of PSCs.¹²⁸

Thermally evaporated organic materials like copper phthalocyanine (CuPc), zinc phthalocyanine (ZnPc),^{134,135} metal acetylacetonate complexes,¹²⁹ pentacene,¹³⁶ and 1,4,5,8,9,11-hexaazatriphenylhexacarbonitrile (HATCN)¹³⁷ can function as buffer layers if the TCO deposition power density is low enough. Figure 10 shows the chemical structures of such commonly used organic buffer layers. The sputter damage on the robust and chemically inert organic molecules such as CuPc and 3,4,9,10-perylene tetracarboxylic dianhydride (PTCDA) is limited. This resilience is usually attributed to the dissipation of collision energies among several neighboring lattice molecules.¹³⁴ Moreover, the electron injection from ITO to the lowest unoccupied molecular orbital of the organic semiconductor was reported to occur via a high density of sputter-induced mid-gap defect states in the buffer layers. Since CuPc absorbs light in the visible range, an alternative layer of BCP was also incorporated as a buffer layer for top illuminated or emitting devices. Figure 10B summarizes the normalized absorbance spectrum of common organic buffer layers.¹³⁸ The

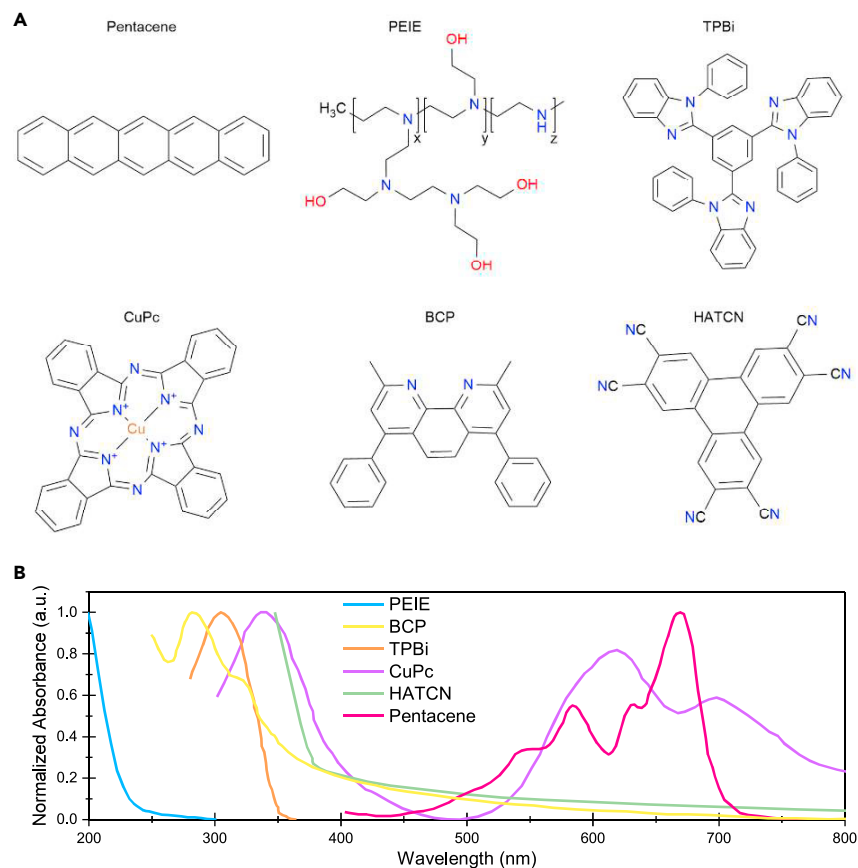


Figure 10. Organic compounds commonly used as buffer layers in optoelectronic devices

(A) Chemical structures of various organic buffer layers used in solar cells and LEDs.

(B) Normalized absorbance spectrum of various thin films used as organic buffer layers (PEIE/quartz,¹³⁹ BCP/ITO/glass,¹⁴⁰ TPBi/fused silica,¹⁴¹ CuPc/glass,¹⁴² HATCN/quartz,¹⁴³ Pentacene/glass¹⁴⁴).

replacement of CuPc with the BCP buffer layer was particularly beneficial for red-emitting OLEDs. We note that in both CuPc and BCP buffer layers, ITO was sputter-deposited at a relatively low rate of 0.3 Å/s, respectively.

Further, the injection efficiencies in both the devices were shown to improve upon deposition of a ~ 3 Å and ~ 5 to 10 Å Li layer between the CuPc and ITO and the BCP and ITO, respectively.^{145,146} As an alternative, an equivalently thick (43 nm) pentacene film has been reported as a buffer layer for protection against sputter damage; however, this resulted in a lower device efficiency due to the strong parasitic absorption of light in pentacene.¹³⁶ Also, the surface morphology of planar molecules, e.g., pentacene, forms polycrystalline films, which affect the growth of ITO on top of it and consequently limit the conductivity and transparency of the overlying ITO. To overcome this limitation, a thin layer of spin-coated PEDOT:PSS onto pentacene can reduce the surface roughness and provide better ITO growth.¹⁴⁷ Although transparent OLEDs containing CuPc or pentacene buffer layers achieved up to 80% optical transparency, both materials exhibit substantial absorption losses in the VIS spectrum. Therefore, another buffer layer, such as nickel acetylacetonate, offers negligible absorption in the VIS range with good electron injection properties analogous to the CuPc buffer layer, resulting in better device performances in

OLEDs (Figure 9D).¹²⁹ HATCN is also reported to be a buffer layer with an impressive hole injection property and chemical stability against oxygen.¹³⁷ Owing to its high transparency in the visible spectrum and a low refractive index of ~ 1.7 , the HATCN buffer layer has been extensively used in inverted OLED devices.^{137,148–150} In addition, its planar discoid shape allows it to be stacked densely on the substrate when thermally evaporated. Taking this advantage, OSCs with an HATCN buffer layer exhibited promising device performance on par with their metal-oxide counterparts, as shown in Figure 9E.⁸⁶ These organic molecules carry a high potential to be applied as a buffer layer in PSCs and OSCs, which is an opportunity yet to explore.

Further, vacuum-evaporated materials may show better tolerance to particle bombardment in the TCO sputtering process than their solution-processed counterparts.¹³⁰ For instance, comparing the spin-coated and thermally evaporated C_{60} , the surface potential of the C_{60} layer shifts ~ 36 mV for evaporated ones and ~ 378 mV for the solution-processed counterparts, according to Kelvin probe force microscopy measurements (Figure 9F). The substantial increase in defect densities at the interfaces of solution-processed layers due to the bombardment (as indicated by the shift of surface potential) accounts for significant variations in reported device performances.¹³⁰ Still, one of the disadvantages of thermally evaporated buffer layers is their rougher surface morphology and requirement of specific thickness values (in general >10 nm) to have continuous and pin-hole-free films, which is needed for adequate protection against sputter damage. Therefore, several previous studies focused on the critical role of film thickness.^{151,152} The common observation from these experiments is insufficient protection if the film is too thin or an increase in series resistance if the film is too thick. To conclude, TE offers solvent-free and physical deposition of buffer layers without involving high energetic particles. This simplicity makes the technique suitable for buffer-layer deposition, but achieving continuous ultrathin films with high optical transparency is still open to further investigation.

Chemical vapor deposition techniques

For conformal and pinhole-free buffer layers on complex surfaces, CVD-based techniques offer unique advantages. For instance, ALD, the most widely used technique for buffer layers among all CVD techniques, involves thin-film formation based on sequential, self-limiting chemical reactions of the precursors. During film growth, the adsorption of precursor on the substrate is a nondirectional process driven by diffusion, creating excellent coverage on all surfaces, a desirable property to form a continuous film.¹⁵³ In contrast, if self-limiting behavior cannot be achieved, the overall process is termed pulsed CVD.¹⁵⁴ The combination of low-temperature processability and sub-nanometer thickness control makes ALD an ideal “soft” deposition technique for buffer layers (Figure 7).¹⁵⁵ More importantly, ALD is adaptable for mass production since it allows the deposition of multiple substrates in cassettes in a single batch. The precursor choice must be a critical step to let the film grow at low temperatures, and this precursor should not be reacting with the underlying layers. Also, processes usually require hydroxyl ($-OH$) groups on the underlying layer to initiate film growth. Therefore, sometimes different surface treatments, such as UV-ozone exposure (if applicable without damage)¹⁵⁶ or utilization of ultrathin nucleation layers might be needed.¹⁵⁷ For instance, inserting $-OH$ -rich PEIE layers as a base layer for ALD films results in denser films on soft layers and brings additional advantages in terms of chemical resistance of such coatings.⁹⁴ Currently, the main drawback of conventional ALD is its relatively slow deposition rate and the high capital investment of the equipment. For mass production, spatial ALD can provide a higher deposition rate

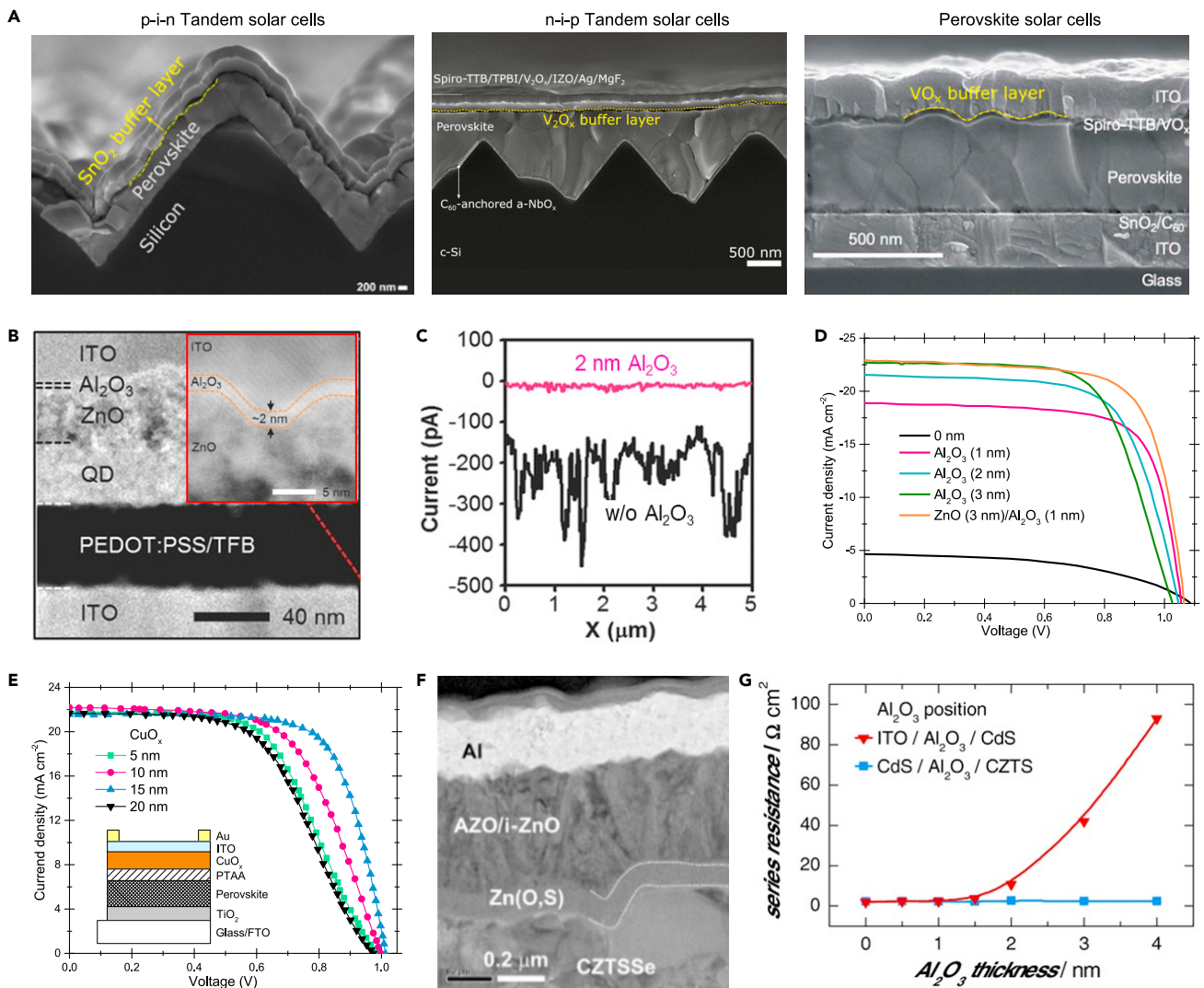


Figure 11. Chemical vapor deposited buffer layers in optoelectronic devices

(A) Cross-sectional SEM images of ALD SnO_2 and VO_x buffer layers used in various single-junction and tandem solar cells. SnO_2 image was reprinted with permission from Aydin et al.⁵² Copyright 2020, Springer Nature. V_2O_x image of tandem configuration was reprinted from Aydin et al.¹⁶³ V_2O_x image of single-junction perovskite solar cell was reprinted with permission from Raimo et al.¹⁶¹ Copyright 2019, The Royal Society of Chemistry.

(B) Transmission electron microscopy images of transparent QLEDs with ALD deposited Al_2O_3 buffer layer and sputtered ITO films. The inset in the red square shows the magnified image of a sputtered ITO/ALD Al_2O_3 /ZnO section (Note: The scale bar in the inset represents 5 nm).

(C) Current distribution of ITO/HTL/QDs/ZnO/ Al_2O_3 structures (shown in B) characterized by conductive atomic force microscopy. Reprinted with permission from Choi et al.⁸⁰ Copyright 2017, Wiley-VCH.

(D) Current-voltage characteristics of semitransparent PSCs with ALD Al_2O_3 buffer layer in different thicknesses and ALD Al_2O_3 /ZnO bilayer. Adapted from Rajbhandari et al.¹⁶²

(E) Current density versus voltage curves of semitransparent perovskite devices with varying buffer thickness of CuO_x . Inset shows the device structure used for measurements. Adapted from Eom et al.¹⁶⁴

(F) Cross-sectional transmission electron microscopy images of CZTSSe solar cells with atomic layer deposited Zn(O, S) buffer layer. Reprinted with permission from Hong et al.¹⁶⁵ Copyright 2016, Elsevier Inc.

(G) Series resistance values of CZTSSe devices were plotted as a function of ALD Al_2O_3 layer thickness for both passivation (on CZTSSe) and buffer layer (on CdS). Reprinted with permission from Lee et al.⁶⁷ Copyright 2016, Wiley-VCH.

thanks to separating the precursors in space rather than in time. For spatial ALD, highly volatile precursors are needed, which may limit the choice of buffer-layer materials. Pulsed ALD can accelerate the process, but it should be noted that pulses might damage the soft layers.¹⁵⁸

Thanks to the advantages mentioned above, ALD metal oxides have found several applications in optoelectronic devices. For instance, SnO_x and ZnO-based buffer layers are frequently utilized in PSCs and perovskite/silicon tandem solar cells if the light is incident on the *n*-type contact side,^{53,55,159,160} whereas VO_x is used if the light is incident from the *p*-type contact side (see examples for solar cells in Figures 11A).¹⁶¹ Although diverse *n*-type metal-oxide materials are available (such as TiO_x , Nb_2O_x , and In_2O_x), SnO_x is still dominant due to its broadband transparency, relatively high carrier concentration, therefore, high conductivity, and high chemical stability.⁵⁸ Alternatively, ultrathin Al_2O_3 also can be used as a buffer layer. Al_2O_3 is a highly insulating material, but after carefully reducing its thickness, it can function as a buffer layer, as reported in QLEDs and PSCs (Figures 11B–11D).^{80,162} An ALD Al_2O_x layer as thin as 2 nm inserted between the charge transport layer and sputtered ITO in QLEDs was reported (Figures 11B), preventing plasma damage and thus enabling remarkably enhanced device operational lifetimes (from less than 1 h to over 23 h).⁸⁰ In addition, such ALD Al_2O_x buffer layers significantly improved the areal homogeneity of the current distribution and prevented short-circuiting the devices (Figure 11C), resulting in total luminance (sum of bottom and top emission) of $73,000 \text{ cd m}^{-2}$ at 9V, which was among the highest at that time. Similarly, ALD Al_2O_x buffer layers have been utilized to improve device performances of PSCs, as shown in Figure 11D.¹⁶²

In general, the optoelectronic properties of ALD buffer layers can be tuned to some extent by processing temperature and pulse-purge conditions in the ALD.¹⁶⁶ Among the transition metal oxides, V_2O_x seems an ideal material since only V_2O_x appears to have a precursor solution that allows for deposition at a temperature below 100°C .^{161,167,168} Low processing temperatures are critical for “sensitive” layers such as metal-halide perovskites due to their degradation at higher temperatures ($>80^\circ\text{C}$, usually by the release of organic cations, e.g., MA^+).¹⁶⁹ The successful application of ALD V_2O_x buffer layers has been demonstrated for *n-i-p* perovskite/silicon tandem and single-junction solar cells (see Figure 11A).^{161,163}

Furthermore, ALD allows for achieving more complex buffer-layer materials, such as ternary ZnSnO (ZTO), which has been successfully demonstrated in PSCs.¹⁷⁰ An ultrathin bilayer of SnO_x and ZTO exhibits better buffer-layer behavior in which the SnO_x prevents the penetration of zinc into the perovskite layer, while the ZTO provides a low-contact resistance with ITO.^{50,170} The benefits of the ALD buffer layer become more vital, especially for all-perovskite and perovskite/organic tandem solar cells, where the recombination junction must be deposited on top of a high bandgap absorber to interconnect the sub-cells electrically.^{171,172} For instance, the ALD bilayer of SnO_x -ZTO can protect the sputtering process of the ITO recombination junction layer.¹⁷³ Moreover, ALD encapsulation layers (ZrO_x and Al_2O_x) are widely employed in OLEDs,¹⁷⁴ and were recently demonstrated to be feasible in PSCs using low-temperature processes.¹⁷⁵ Despite its successful application in solar cells, using an ALD buffer layer in inverted OLEDs, OSCs, and QDSCs has not been explored yet and is worth further investigation.

Atmospheric pressure CVD (AP-CVD) is an excellent alternative to conventional ALD for fast and cost-efficient processing.¹⁶⁴ Although ALD and AP-CVD use similar precursors, the AP-CVD technique mixes precursors in the gas phase to obtain CVD rather than self-limiting growth, which accelerates the growth of the film. For a simple comparison, 15 nm of CuO_x can be acquired by pulsed CVD within 24 min, whereas it would take 4 h by conventional ALD to obtain the same material.¹⁶⁴ Like ALD, this method forms thin films by the reaction of precursors either in the gas phase or on the substrate’s surface, but AP-CVD does not require a high vacuum. Despite these advantages, few studies have been demonstrated to fabricate buffer

layers via AP-CVD. For *p*-type materials, successful plasma-damage protection by CuO_x buffer layers of *n-i-p* PSCs has been reported (Figure 11E).¹⁶⁴ This can be an excellent alternative to ALD V_2O_x and thermally evaporated MoO_x buffer layers, owing to the high transparency in the infrared region of CuO_x and its high thermal stability under operation. Moreover, its processability at 100°C with the CVD method makes it suitable for several temperature-sensitive optoelectronic devices.³⁸ For *n*-type materials, ZnO , TiO_x , and SnO_x have been implemented with the AP-CVD method.¹⁷⁶ It should be noted that the growth rate usually follows an inverse trend with the temperature, and high temperatures might be harmful to the devices. For instance, processing above 110°C is reported as harmful for perovskite layers since the organic cation leaves from the surface at high temperatures.¹⁵⁸ Hence, the deposition rate (and therefore processing temperature) should be set considering the temperature sensitivity of the soft layers.

In thin-film CZTSSe and CIGS solar cells, ALD is widely used to enable conformal coating of buffer layers on rough surfaces of absorber layers (Figure 11F). CIGS devices with CBD $\text{Zn}(\text{O}, \text{S})/\text{ALD } \text{Zn}_x\text{Mg}_{1-x}\text{O}$ double-buffer layers hold the current record PCE of 23.5%.^{99,165,177} In addition, insertion of a thin layer of ALD Al_2O_x (0.5 nm) between CdS and ITO may protect CdS against sputtering damage and thus reduce V_{OC} deficit in CZTSSe devices; however, careful tuning of Al_2O_x thickness is needed to avoid a severe increase in series resistances, as depicted in Figure 11G.⁶⁷

STRATEGIES FOR TRANSPARENT ELECTRODE DEPOSITION TO ELIMINATE BUFFER-LAYER USAGE

Sputtering process optimization and new sputtering hardware design

Rather than using an additional buffer layer, adding processing costs, several approaches have been discussed to minimize the sputtering damage on sensitive layers. These efforts include lowering the power density,¹⁷⁸ changing the sputter gas or gas pressure,^{76,179} using facing-target sputtering (FTS),¹⁸⁰ and combining low- and high-power sputtering in a two-step process.^{123,181}

For magnetron sputtering (as sketched in Figure 12A), there is no consensus on which power density value can result in a damage-free deposition. For instance, the power density of 0.07 W cm^{-2} (40 W with a 507 cm^2 ITO target) has been reported as not causing damage to spiro-OMeTAD in PSCs.¹⁷⁸ On the other hand, an RF power density of 0.4 W cm^{-2} enabled the deposition of ITO directly on PTAA without causing damage, which may be a good benchmark for further development.¹⁷⁸ Generally, the power density for sputtered TCOs used in PSCs varies from 0.76 W cm^{-2} to 4.4 W cm^{-2} .^{12,38} Target-to-substrate distance, sputtering gas, and process pressure are essential parameters among others to consider to reduce the power density threshold. Regarding the effect of background gas during sputtering, a replacement of Ar with Kr has been shown to reduce the kinetic energy of sputtered atoms, as revealed in a more significant photoluminescence intensity BAQ deposited in Kr than those deposited in Ar gas.¹⁷⁹ Besides the gas composition, an increase in the total gas pressure can lower the kinetic energy of atomic particles by minimizing the energy of sputtered particles.¹⁷⁹ Another approach to overcome the heating issue on the sensitive films is intermittent sputtering deposition sequence. For instance, opening the shutter for 1 s every 7 s during the deposition enables direct sputtering on metal acetylacetonate complexes without thermal damage.¹²⁹

Additionally, post-annealing the device stack after sputtering at mild temperatures (such as $\sim 90\text{--}100^\circ\text{C}$) might help mitigate the S-shape *I-V* curve behavior. The short

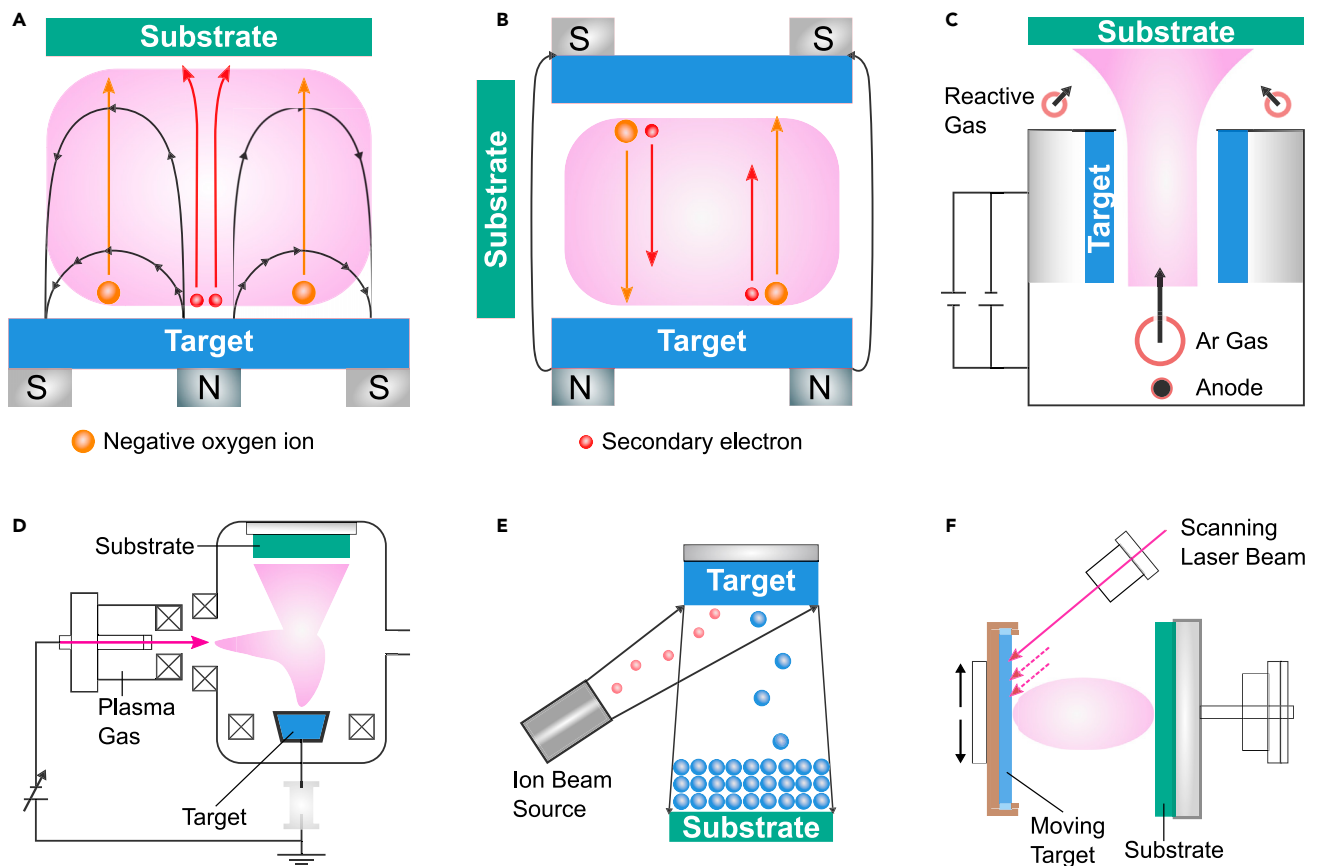


Figure 12. Schematic demonstrations of alternative advanced sputtering designs and other alternative PVD techniques for “soft-landing” deposition

- (A) Magnetron sputtering.
- (B) Facing target sputtering.
- (C) Gas-flow sputtering system.
- (D) Reactive plasma deposition (hollow cathode ion plating).
- (E) Ion beam sputtering.
- (F) Pulsed laser deposition.

annealing step can passivate the shallow trap states deeper in the perovskite layer by the diffusion of PCBM into the grain boundaries of the perovskite film. A similar approach of post-annealing after direct growth of ITO (sputtering at 1.1 W cm^{-2} power density) onto spiro-OMeTAD achieved the most efficient buffer-layer-free semi-transparent PSCs (PCE of 15.7%) at that time.¹⁸²

Although several successful attempts of direct TCO sputtering on top of transport layers have been demonstrated, most studies on sputtering damage in optoelectronic devices have been primarily focused on linking the external process parameters to the device performance. However, establishing these correlations to the plasma parameters such as the ion energy may serve as a basis for a more systematic approach toward the TCO deposition optimization. As discussed in the section “origins of damage during magnetron sputtering of TCOs,” negative ions are the most energetic species and are strong candidates to be the primary source of degradation. Therefore, one crucial milestone to enable damage-free deposition of transparent electrodes with the desired optoelectronic properties and acceptable deposition rates using the current magnetron sputtering processes lies in mitigating the bombardment by negative ions. There are

two possible strategies to follow: (1) lowering the target voltage during the sputtering and (2) physically separating the target from the substrate.

Enhancing the plasma density can be partially achieved by tuning the processing parameters. For instance, monitoring the target voltage may give insights into reducing the maximum kinetic energy of the negative oxygen ions. It was previously shown that lowering the power density⁴⁰ and increasing the process pressure¹⁸³ leads to the decreased discharge voltage, which agrees with the reported observations from the device reports as discussed above. However, the preferred and more efficient way to lower the target voltage without compromising the deposition rate and sputtering yield would be to increase the ionization of the plasma without additional negative ions acceleration. These may require upgrading the existing hardware, such as follows:

1. RF plasma excitation.¹⁸⁴ Preferably, switching to higher RF frequencies such as 27.12 MHz.¹⁸⁵
2. Use of rotatable magnetrons⁶² (and/or stronger magnets⁴⁰ for existing sputtering systems).

Another approach lies in placing substrates, not in direct sight of the target. This also implies modified designs of the currently used magnetron sputtering equipment to the following configurations:

1. FTS¹⁸⁶
2. Gas-flow sputtering (GFS)¹⁸⁷ or hollow cathode sputtering
3. Off-axis sputtering^{188,189}

For instance, FTS has no direct irradiation of a high-density plasma on the device (unlike conventional sputtering), offering possibilities to reduce damage during TCO deposition.⁷⁷ A magnet is applied behind two targets that form a homogeneous magnetic field to limit the charged energetic particles (see the sketch in Figure 12B). Thus, the charged electrons and ions move perpendicularly between the targets. The substrate, placed out of the plasma region, is not directly affected by the strike of high energetic particles.^{180,190} The average energy of atoms bombarding the substrate in FTS is around 0.2 to 0.5 eV due to the short mean free path in the plasma region, which is much lower than conventional sputtering.^{39,42} As severe bombardment is absent during FTS, neither thermally induced degradation nor defects occur to the organic layer.^{45,181,191}

The two-step linear FTS process of InZnSnO (IZTO) top electrode for semitransparent PSCs is an excellent example of this.¹⁸¹ A slow sputtering (low damage) process followed by a fast sputtering method in the second step results in a higher deposition rate of FTS (44 nm min⁻¹) than conventional sputtering of ITO (20 nm min⁻¹). Moreover, two-step RF sputtering (50 W/150 W) of an IZO top electrode applied to transparent QLEDs, led to performances better than standard one-step sputtering of IZO (150 W) and on par with nondestructive evaporated Al counterparts.¹⁹² Similarly, this technique is used for ITO top electrode deposition in OLEDs to prevent severe sputtering damage.^{123,193,194} The suppression of damage in FTS can be further improved by inserting the shield plates near the targets and generating a magnetic field from magnets near the substrate holder.¹⁹⁰ This modification effectively restrains the incidence of the secondary electrons on the substrate when the top ITO layer is deposited in an OLED device.^{180,190}

As mentioned previously, hollow cathode glow discharge, resulting in high plasma densities, may be advantageous for “soft-landing” deposition. For instance, in GFS, ejected particles are thermalized and carried toward the substrate by an intense gas flow (Figure 12C). GFS was shown to cause a smaller decrease in c-Si passivation quality than DC sputtering as relevant for application in SHJ cells.⁴⁵ This may also be attributed, in part, to the high working pressure during GFS (typically in the mbar range).

Another hollow cathode-based method is reactive plasma deposition (also known as hollow cathode discharge ion plating), shown in Figure 12D. In contrast to the magnetron sputtering, it operates in arc mode rather than a glow discharge, ensuring lower working voltages. Furthermore, reactive plasma deposition (Figure 12D) has been successfully utilized to fabricate ZnO-based and W-doped In_2O_3 transparent electrodes for CIGS and SHJ applications.^{195,196}

In summary, combining a softer sputtering technique, a two-step process, and/or a mild thermal posttreatment could be the cornerstone of depositing an electrode onto perovskite, organic layers, or QDs.

Alternative “soft-landing” techniques for transparent conductive oxide deposition

While the sputtering damage can be reduced by modifying the deposition processes, alternative soft-landing deposition methods can eliminate the buffer-layer usage. Ion beam sputtering (IBS) and PLD have also been investigated among PVD methods for damage-free TCO deposition for optoelectronic devices. High-performing ITO deposited by IBS (see the sketch in Figure 12E) on PET substrates at low temperatures ($<150^\circ\text{C}$) was implemented in flexible OLEDs as the front electrode.¹⁹⁷ Unfortunately, there are very limited studies on IBS deposition on top of functional layers. Previously, damage-free deposition of Al by IBS for blue bottom-emitting OLEDs was demonstrated.¹⁹⁸ The impact of high-energy particles is partially mitigated thanks to the tool's geometry, where the substrate is only exposed to the secondary electrons from the target. In contrast, the plasma is only contained in the ion source. In the same work, magnetic traps were successfully implemented to significantly reduce charge particle impingement as measured by a cylindrical energy analyzer.¹⁹⁸ On the other hand, an indium oxide (In_2O_3) capping layer was deposited on top of transparent OLEDs via modified two-step IBS method, in which argon and oxygen ion sputtering were sequentially employed to obtain bilayer 5 nm/95 nm In_2O_3 films, where the role of the first layer is to reduce damage to, and prevent oxidation of, underlying layers.¹⁹⁹

PLD, in its turn (Figure 12F), has an advantage of the near-stoichiometric transfer of target compounds and has also been demonstrated as an alternative technique for damage-free deposition in solar cells and LEDs. Room temperature PLD-deposited IZRO applied as a rear electrode in buffer-free semitransparent PSCs enabled higher efficiencies (15.1%) than those with sputtered ITO (11.9%).²⁰⁰ The standard PLD of TCOs as top electrodes for OSCs was reported to still lead to substantial impact damage to the organic layers by high-energy particles during deposition.²⁰¹ Alternatively, eclipse PLD (whereby a circular shadow mask with a diameter of 19.4 mm is installed between the target and the sample) in an Ar atmosphere to prepare the top electrode of OSCs could enable devices with efficiencies similar to the reference device, which employed a thin metal electrode. Moreover, AZO-based TCOs fabricated by PLD were implemented on CIGS solar cells and OLEDs as transparent top electrodes; however, both devices utilized buffer layers (CdS/ZnO for CIGS cells,

WO_x for OLEDs) to mitigate process damage.^{202,203} Current experimental evidence suggests that the success in developing damage-free deposition by PLD lies in reducing the energy of the arriving species through thermalization via the background gas at elevated deposition pressures (compared with sputtering). This is enabled by a more extensive choice of process pressure, as the source of the material ablation (excimer laser) is physically decoupled from the vacuum chamber. However, other potential effects such as possibly intrinsically different ion energy distributions during laser ablation or smaller plasma imprint on the substrates due to the highly confined PLD plasma are much less studied and cannot be entirely discarded.

As mentioned in the previous section, CVD-based techniques, mainly ALD, are attractive candidates for the buffer layers and damage-free deposition of the transparent electrodes themselves. So far, high-quality AZO, IZO, and ITO layers have been prepared by ALD on glass substrates.^{204,205} Studies have shown that the desired materials can be deposited at a range of temperatures known as “ALD temperature windows” depending on the precursors used. The deposition within the ALD temperature window is needed to obtain the desired material properties comparable to those deposited via conventional sputtering. For example, ALD deposited AZO top electrodes were successfully implemented on OLEDs.²⁰² As discussed above, the optimum processing temperature of AZO at 150°C is a challenging ALD application for thermally vulnerable materials such as organic or perovskite compounds, which implies that alternative precursors should be studied. Also, plasma-enhanced ALD (PE-ALD) can obtain high-quality materials at lower temperatures, but one must consider how this process might affect the device. Reports on PE-ALD for top electrodes are limited so far and warrant further work.²⁰⁶ Also, conventional ALD is usually considered a slower deposition technique than sputtering, specifically for thick films. Spatial ALD, in which the precursors are separated in space rather than in time, may accelerate the processing speed for TEs. On the other hand, B-doped ZnO layers have been implemented by metal-organic CVD (MOCVD) to SHJs as an alternative TCO to sputtered ITO, exhibiting good optical properties while having some electrical drawbacks due to aging of the layers, which can be solved by further studies and might be a promising technique to replace sputtering.²⁰⁷

CONCLUSION AND OUTLOOK

Beyond the state-of-the-art, buffer-layer/TCO stacks hold great promise for applications where high transparency and (semi)conductivity are needed, not only for LEDs and PVs, but also a wide range of applications such as semitransparent conductors, field-effect transistors, thermal shields, and photo-detectors, to name a few. However, the frequently used magnetron sputtering method for the transparent electrodes causes inevitable damage to soft layers such as perovskites and organic films. The insertion of an underlying buffer layer is still the most preferred solution to limit or mitigate the effects of sputter damage, and while there is no universal buffer-layer material and no preferred deposition technique, our review provides cross-field learnings to explore different materials for the specific device application.

We argue that optimization of the sputtering process, as the most established mean of fabricating transparent electrodes, has not yet been fully explored. Linking plasma properties to the interface degradation may be the pathway to deeper understanding and associated device improvements, potentially eliminating the requirement for the buffer layer. In general, effort should be focused on mitigating

the highly energized particles during sputtering. This can be achieved by increasing the plasma ionization and/or changing the tool geometry to minimize the plasma imprint on the substrate, such as FTS or GFS.

For the development of alternative TCOs, the previously counted key criteria need to be satisfied, regardless of the deposition technique. Several emerging techniques, such as PLD, IBS, or ALD, fulfill some of these criteria. However, sufficient throughput should be verified to employ the full potential of these techniques in mass production. ALD seems to be the most advanced technology that allows low-temperature deposition and produces conformal thin films. In this case, research effort should be put into finding alternative precursors to allow for low deposition temperatures. In addition, the use of remote plasma ALD might be worth investigating. In the future, more work needs to be done to make these processes comparable to commercial sputtered TCOs. We foresee that the potential of buffer-free devices will only be realized when more research activities are devoted to this direction.

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AUTHOR CONTRIBUTIONS

Conceptualization, E.A.; writing – original draft, E.A., C.A., and M.A.Y.; writing – review & editing, E.A., C.A., Y.S., M.A.Y., K.P.S.Z., A.P., Y.F., and T.G.A.; funding acquisition, T.D.A., H.J.B., M.M.-M., and S.D.W.; supervision, T.D.A., H.J.B., M.M.-M., and S.D.W.

DECLARATION OF INTERESTS

The authors declare no competing interests.

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